

Individual Pitch Control for Mitigation of Power Fluctuation

Mahesh Thati & Mahesh Jonnala

¹Assistant Professor, Dept of EEE, Institute of Aeronautical Engineering college, Dundigal, Hyderabad.

E-mail:maheshthati216@gmail.com

²Masters in Power Electronic Systems from Osmania University, Hyderabad.

E-mail:mahesh.vikram023@gmail.com

ABSTRACT:Due to the wind speed variation, wind shear and tower shadow effects, grid connected wind turbines are the sources of power fluctuations which can turn out flicker throughout continuous operation. This paper presents an individual pitch control (IPC) strategy to mitigate the wind turbine power fluctuation at both above and below the rated wind speed conditions. Three pitch angles are adjusted separately according to the generator output power and the azimuth angle of the wind turbine. The IPC strategy scheme is proposed and the individual pitch controller is designed. The simulations are performed on the NREL (National Renewable Energy Laboratory) 1.5MW upwind reference wind turbine model. The simulation results are presented and discussed to show the validity of the proposed control method.

KEYWORDS-wind turbine; IPC; power fluctuation; FAST

I. INTRODUCTION

Presently the reality vitality interest may be expanding because of number development and up to date modern culture persuading a considerable measure of ventures done elective vitality wellsprings for example, Solar, Wind, bio-mass, energy units etc; "around the renewable vitality sources, wind vitality reliably demonstrates its great possibility to serve Similarly as clean What's more boundless vitality wellspring. For the increment about wind control infiltration under the grid, the energy caliber gets to be a critical issue. We quit offering on that one essential part from claiming force nature may be flicker since it might turn into a restricting component for coordination wind turbines under feeble grids, Furthermore actually under generally solid grids assuming that the wind force infiltration levels

are secondary. Flicker is characterized as "an feeling of precariousness for visual sensation prompted. Toward a light stimulus, whose luminance or ghastrly conveyance oscillates with time". Flicker may be prompted toward voltage fluctuations, which need aid initiated by load stream transforms in the grid. Grid-connected variable velocity wind turbines are fluctuating force sources Throughout constant operation. The force variances created by wind pace variation, wind shear, tower shadow, yaw errors, and so on. prompt those voltage variances in the network, which might transform flicker. Separated from the wind control wellspring conditions, the control framework aspects likewise bring effect on flicker emanation about grid connected wind turbines, for example, such that impedance point. The flicker emanation for diverse sorts for wind turbines will be exactly different. In spite of variable-speed wind turbines are better regarding the flicker emission than fixed-speed wind turbines, with the large increase of wind power penetration level, the flicker study on variable speed wind turbines becomes necessary and imperative. Previously there are number of ways to reduce the flicker in power generated. These are implemented by using reactive compensation. When the grid has a very low impedance angle ie 100 these techniques will be redundant. For a large distributive networks the reactive power needed for compensation will be as greater as 3.26 pu which is practically not possible to generate from STATCOM especially when DFIG is present in the system.

Another way by controlling the active power by varying the DC link capacitance can be used for reducing flicker but this requires a large capacitance which is of high cost and reduces the life of capacitor in storing the energy. Pitch actuating system can also be used for mitigation of flicker but time delay and

pitch rate great affects the system. This effect is considerably large in case of variable speed turbines. As a result of above mentioned drawbacks of existing solutions there is a need to find an alternative solution for power fluctuation mitigation. A novel scheme used in helicopter industry for load reduction is applied to wind turbine. That is pitching the blades individually as per the wind speed and direction of wind flow. IPC is a promising solution for reducing power oscillation in active power generation in case of distributive network systems.

II. POWER FLUCTUATION ANALYSIS

Power generated by wind turbines is much more variable than that produced by conventional generators. The power fluctuations are due both to stochastic processes that determine wind speed at different times, and to periodic processes that are referred to as wind shear and tower shadow. Wind shear is used to describe the variation of wind speed with height while tower shadow describes the redirection of wind due to the tower structure [4].

Wind shear: The increase of wind speed with height is known as wind shear. A common wind shear model, shown as (1), is taken directly from the literature on wind turbine dynamics [4].

Tower shadow: Today most wind turbines are constructed with a rotor upwind of the tower to reduce the tower interference of the wind flow. In the upwind rotor case, the wind speed V_t considering tower shadow effect can be modeled using potential flow theory [4].

A. Total aerodynamic torque

Fig. 1 illustrates the overall wind turbine aerodynamic torque, which obviously shows the $3p$ effect, and also the aerodynamic torque has the maximum drop when one of the three blades is directly in front of the tower.

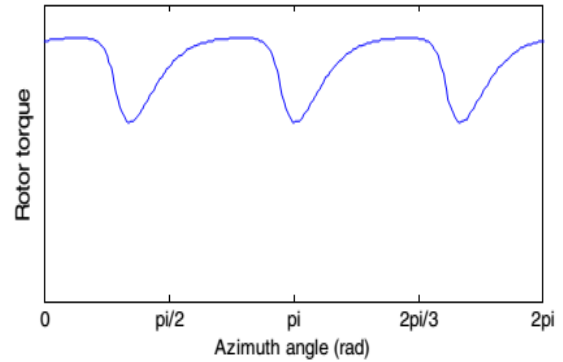


Figure 1. Aerodynamic torque involving $3p$ effects

III. SYSTEM CONFIGURATION

The overall scheme of DFIG based wind turbine system is shown in Fig 2, which consists of a wind turbine, gearbox, DFIG, a back-to-back converter which is composed of rotor side converter (RSC) and grid side converter (GSC) and a dc link capacitor as energy storage placed between the two converters. In this paper, turbulent wind is simulated by TurbSim. Wind turbine code FAST is used to simulate the mechanical parts of wind turbine and the drivetrain. The pitch and converter controllers, DFIG, and power system are modeled by Simulink blocks.

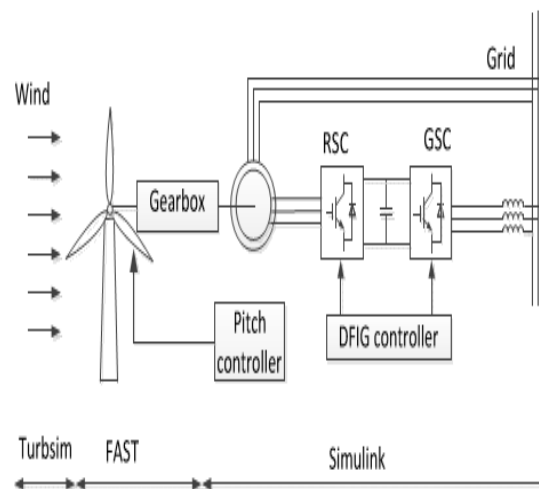


Fig. 2. The overall scheme of the DFIG based wind turbine system

A. TurbSim and FAST

TurbSim and FAST are developed at the National Renewable Energy Laboratory (NREL) and they are accessible and free to the public. TurbSim is a stochastic, full-field, turbulent-wind simulator. It numerically simulates time series of three-dimensional wind velocity vectors at points in a vertical rectangular grid. TurbSim output can then be used as input into FAST [5]. The open source code FAST can be used to model both two and three bladed, horizontal-axis wind turbines. It uses Blade Element Momentum (BEM) theory to calculate blade aerodynamic forces and uses an assumed approach to formulate the motion equations of the wind turbine. For three-bladed wind turbines, 24 DOFs (Degree of Freedom) are used to describe the turbine dynamics. Their models include rigid parts and flexible parts. The rigid parts include earth, base plate, nacelle, generator, and hub. The flexible parts include blades, shaft, and tower. FAST runs significantly faster than a large comprehensive code such as ADAMS because of the use of the modal approach with fewer degrees of freedom (DOFs) to describe the most important parts of turbine dynamics.

B. Mechanical Drivetrain

In order to take into account the effects of the generator and drivetrain to the wind turbine, two-mass model is used which is suitable for transient stability analysis [6] shown in Fig. 3. The drivetrain modeling is implemented in FAST, and all values are cast on the wind turbine side.

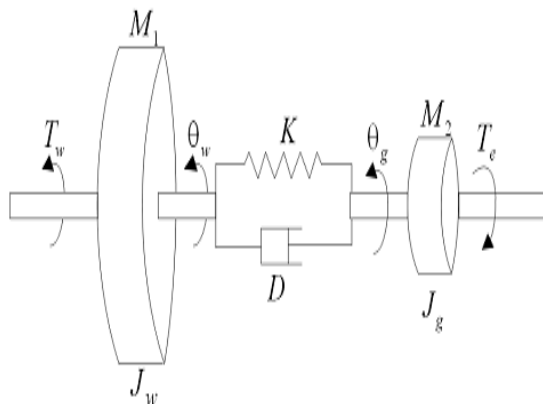


Figure 3. Two-mass model of the drivetrain

C. DFIG model and converters control

The model of the DFIG in Simulink is based on d-q equivalent model. All electrical variables are referred to the stator. Vector control techniques are the most commonly used methods for back to back converters in wind turbine system.

Two vector control schemes are illustrated respectively for the RSC and GSC, as shown in Fig. 4. Normally the control objective of RSC is to implement maximum power tracking by controlling the electrical torque of DFIG, while the objective of GSC is to keep the DC-link voltage constant.

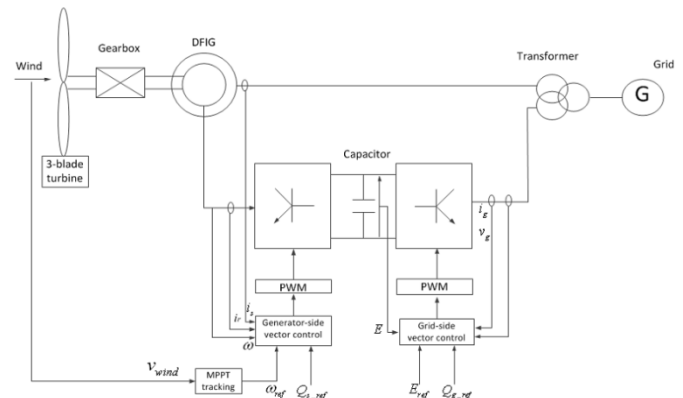


Figure 4. Control diagram of RSC and GSC of grid-connected wind turbine with DFIG

IV. INDIVIDUAL PITCH CONTROL FOR MITIGATION OF WIND TURBINE POWER FLUCTUATION

As illustrated in Fig. 1, the aerodynamic torque will drop three times per revolution, so that the aerodynamic power of the wind turbine as well as the generator output power will also drop three times in a cycle. If the aerodynamic torque can be controlled well to some extent that it will not drop or not drop so prominently when one of the blades is directly in front of the tower, the wind turbine aerodynamic power thus the generator output power will fluctuate

in a much smaller range. When wind speed is above rated wind speed, pitch angles should be tuned by traditional collective pitch control (CPC) to keep the output power at its rated value in order not to overload the system, and normally the 3p effect is not taken into account. For attenuating the power oscillation caused by 3p effect, one of the blade pitch angles can be added by a small pitch increment which is dependent on the wind turbine azimuth angle and the generator output power.

When wind speed is below the rated wind speed, usually the control objective of wind turbine is to implement maximum power tracking by generator electrical torque control. Pitch control is not used in this area. However if the pitch angles can be adjusted around a small average value, the 3p effect can also be reduced. For this purpose, the pitch angle should leave a small amount of residual for pitch movement. This means part of the wind energy will be lost. Based on this control concept, a novel individual pitch control strategy is proposed. The control scheme is shown in Fig. 5.

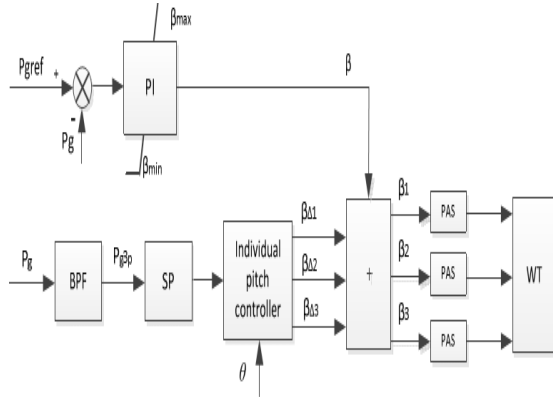


Figure 5. A novel individual pitch control scheme

The control scheme consists of two control loops: collective pitch control loop and individual pitch control loop. The collective pitch control is responsible for limiting the output power. In this loop, P_{gref} is the rated generator power, P_g is the generator output power, β is the collective pitch angle, of which the minimum value β_{min} can be obtained by simulations under different wind speeds such that power fluctuation mitigation may compromise the power loss. In the individual pitch control loop, the BPF (band pass filter) is to let the frequency of 3p

generator active power through and block all other frequencies. P_{g3p} is the 3p component of the generator power, and this component will be sent to the signal processing (SP) block, due to the fact that the power signal has to be transferred to the pitch signal.

In this paper, the wind turbine is simulated by FAST, in which blade 3 is ahead of blade 2, which is ahead of blade 1, so that the order of blades passing through a given azimuth is 3-2-1-repeat. The individual pitch controller will output a pitch increment signal which will be added to the collective pitch angle for a specific blade, dependent on the blade azimuth angle. The principle of the individual pitch controller is described in Table 1.

Azimuth angle θ	$\beta_{\Delta i}$
$0 < \theta < 2\pi/3$	$\beta_{\Delta 2}$
$4\pi/3 > \theta > 2\pi/3$	$\beta_{\Delta 1}$
$2\pi > \theta > 4\pi/3$	$\beta_{\Delta 3}$

V. SIMULATION RESULTS

In order to verify the validity of the proposed individual pitch control strategy, the whole wind turbine system is built in Simulink, and some simulation results are obtained under both high and low wind speeds.

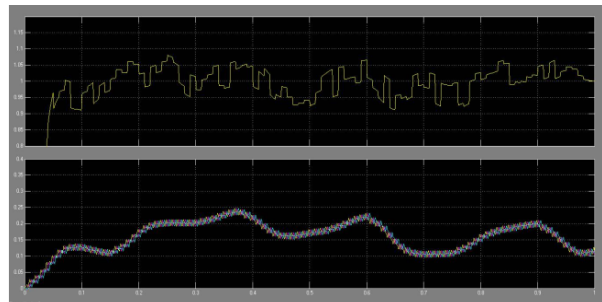


Figure 6 Matlab/simulink result for high wind with IPC scheme

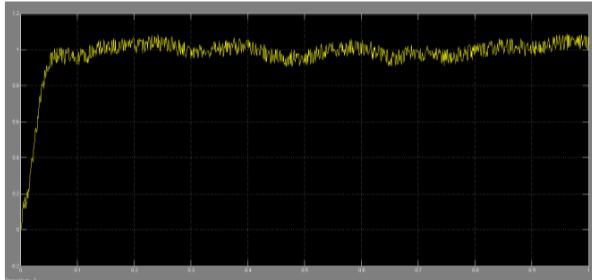


Figure 7 Matlab/simulink result for high wind without IPC scheme

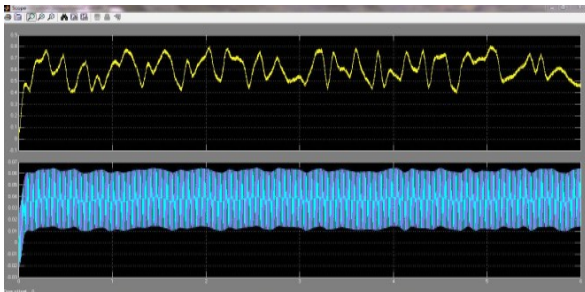


Figure 8 Matlab/simulink result for low wind with IPC scheme

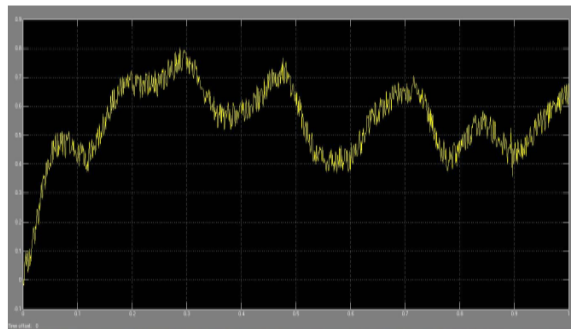


Figure 9. Matlab/simulink result for low wind without IPC scheme

VI. CONCLUSION

This paper designates a technique of flicker mitigation by IPC of variable-speed wind turbines with MW-level DFIG. The MW-level DFIG based variable speed wind turbine system is simulated using Simulink, Turbsim and FAST. A novel individual pitch control method is proposed to mitigate the wind turbine power fluctuation caused by wind shear and tower shadow effects. The individual pitch control scheme is presented and controller is designed. The simulations are performed on the NREL 1.5MW upwind reference wind turbine model.

The simulation results demonstrate the capability of the proposed strategy.

REFERENCES

- [1] B. ChittiBabu, K.B. Mohanty, C. Poongothai, Performance of Double Output Induction Generator for Wind Energy Conversion Systems, Proc. of IEEE First International Conference on Emerging Trends in Engineering and Technology, 2008, pp.933-938.
- [2] T. Sun, Z. Chen, and F. Blaabjerg, "Flicker study on variable speed wind turbines with doubly fed induction generators," IEEE Trans. Energy Conversion, vol. 20, no. 4, pp. 896–905, Dec. 2005.
- [3] W. Hu, Z. Chen, Y. Wang, and Z. Wang, "Flicker mitigation by active power control of variable-speed wind turbines with full-scale back-to-back power converters," IEEE Trans. Energy Conversion, vol. 24, pp.640–649, Sep. 2009.
- [4] D. S. L. Dolan, and P. W. Lehn, "Simulation model of wind turbine 3p torque oscillations due to wind shear and tower shadow," IEEE Trans. Energy Convers., vol. 21, no. 3, pp. 717–724, Sep. 2006.
- [5] B. J. Jonkman, and M. L. J. Buhl. FAST User's Guide. National Renewable Energy Laboratory (NREL), Golden, CO, Tech. Rep. NREL/EL-500-38230, [Online]. Available: <http://wind.nrel.gov/designcodes/simulator/fast/>
- [6] T. Sun, Z. Chen, and F. Blaabjerg, "Flicker study on variable speed wind turbines with doubly fed induction generators," IEEE Trans. Energy Convers., vol. 20, no. 4, pp. 896–905, Dec. 2005.
- [7] K. Yun-Seong and W. Dong-Jun, "Mitigation of the flicker level of a DFIG using power factor angle control," IEEE Trans. Power Del., vol. 24, no. 4, pp. 2457–2458, Oct. 2009.
- [8] W. Hu, Z. Chen, Y. Wang, and Z. Wang, "Flicker mitigation by active power control of variable-speed wind turbines with full-scale back-to-back power

converters,” IEEE Trans. Energy Convers., vol. 24, no. 3, pp. 640–649, Sep. 2009.

[9] E. A. Bossanyi, “Individual blade pitch control for load reduction,” WindEnergy, vol. 6, pp. 119–128, 2002.

[10] E. A. Bossanyi, “Further load reductions with individual pitch control,” Wind Energy, vol. 8, pp. 481–485, 2005.

[11] Y. Zhang, Z. Chen, M. Cheng, and J. Zhang, “Mitigation of fatigue loads using individual pitch control of wind turbines based on FAST,” in Proc. 46th Int. Conf. Universities’ Power Eng., Soest, Germany, 2011.

[12] B. J. Jonkman and M. L. J. Buhl, “FAST User’s Guide,” National Renewable Energy Laboratory (NREL), Golden, CO, USA, Tech. Rep. NREL/EL-500-38230, (2005). [Online]. Available: <http://wind.nrel.gov/designcodes/simulators/fast/>

[13] S. M. Muyeen, M. Hasan, R. Takahashi, T. Murata, J. Tamura, Y. Tomaki, A. Sakahara, and E. Sasano, “Comparative study on transient stability analysis of wind turbine generator system using different drive train models,” IET Renewable Power Generation, vol. 1, no. 2, pp. 131–141, 2007.

[14] A. D. Wright and L. J. Fingersh, “Advanced control design for wind turbines Part I: Control design, implementation, and initial tests,” National Renewable Energy Laboratory, NREL Rep. TP-500–42437, National Renewable Energy Laboratory, Mar. 2008.

[15] Electromagnetic Compatibility (EMC)—Part 4: Testing and Measurement Techniques—Section 15: Flicker meter—Functional and Design Specifications, IEC Std. 61 000–4–15, Nov. 1997.

[16] A. Larsson, “Flicker emission of wind turbines during continuous operation,” IEEE Trans. Energy Convers., vol. 17, no. 1, pp. 114–118, Mar. 2002.

[17] Grid Code 3.2.5 Wind Power Plant above 11 kW. [Online]. Available: <http://energinet.dk/>

BIODATA



Mahesh Thati, a teaching experience of 6 years i.e. from 2012 to 2017 and currently Working as Assistant Professor in Institute of Aeronautical Engineering college, Dundigal, Hyderabad.



Mahesh Jonnala completed Masters in Power Electronic Systems from Osmania University, Hyderabad.