
An Efficient Power Flow Improvement in Transmission Line using UPFC

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Abstract: *A new reactive power coordination controller has been designed to limit excessive voltage excursions during reactive power transfers. The shunt converter of the UPFC controls the UPFC bus voltage/shunt reactive power and the dc link capacitor voltage. The series converter of the UPFC provides simultaneous control of real and reactive power flow in the transmission line the shunt converter has been modeled as a 4-module converter. The series converter consists of two sets of converters. One set of converter is used for the real power flow control and the other set of converter is used for the reactive power flow control. Recent advances in high voltage IGBT technology allow for higher switching frequencies with lower losses. This allows for practical implementation of PWM control. The switching frequency for the converters has been chosen to be nine times the fundamental. Here we use matlab/simulink for the simulation purpose and outputs are verified in the scope.*

Keywords- Flexible AC Transmission System (FACTS), Unified Power Flow Controller (UPFC), PWM, IGBT

I. INTRODUCTION

The power transmitted over an ac transmission line is a function of the line impedance, the magnitude of sending-end and receiving-end voltages, and the phase angle between these voltages. Traditional techniques of reactive line compensation and step-like voltage adjustment are generally used to alter these parameters to achieve power transmission control. Fixed and mechanically shunt and series reactive compensation are employed to modify the natural impedance characteristics of transmission lines in order to establish the desired effective impedance between the sending and receiving-ends to meet power transmission requirements. Voltage regulating and phase shifting transformers with mechanical tap-changing gears are used to minimize voltage variation and control power flow. These conventional methods provide adequate control

under steady-state and slowly changing system conditions, but are largely ineffective in handling dynamic disturbances. The traditional approach to contain dynamic problems is to establish generous stability margins enabling the system to recover from faults, line and generator outages, and equipment failures. This approach, although reliable, generally results in a significant underutilization of the transmission system. As a result of recent environmental legislation, rights-of-way issues, construction cost increases, and deregulation policies, there is an increasing recognition of the necessity to utilize existing transmission system assets to the maximum extent possible. To this end, electronically controlled, extremely fast reactive compensators and power flow controllers have been developed within the overall framework of the FACTS initiative. These compensators and controllers either use conventional reactive components and tap-changing transformer arrangements with thyristor valves and control electronics or employ switching power converters, asynchronous voltage sources, which can internally generate reactive power for, and also exchange real power with, the ac system.

The Unified Power Flow Controller (UPFC) is a member of this latter family of compensators and power flow controllers which utilize the synchronous voltage source (SVS) concept for providing a uniquely comprehensive capability for transmission system control. Within the framework of traditional power transmission system concepts, the UPFC is able to control, simultaneously or selectively, all the parameters affecting power flow in the transmission line. Alternatively, it can provide the unique functional capability of independently controlling both the real and reactive power flow in the line. These basic capabilities make the Unified Power Flow Controller the most powerful device presently available for transmission system control. Unified power flow controller (UPFC) is a member of FACTS family. It is a combination of Static synchronous compensator (STATCOM) and Static

synchronous series compensator (SSSC) coupled via a common dc-link, to allow bi-directional flow of real power between the series output terminals of the SSSC and the shunt output terminals of the STATCOM. The UPFC, by means of angularly unconstrained series voltage injection, is able to control the transmission line voltage, impedance and angle or the real and reactive power flow in the line.

Also the problem of low-frequency power swings is a matter of concern for power systems engineers. As it is becoming increasingly important to fully utilize the existing transmission system assets, proper attention should be given to the enhancement of utilizing the transmission capacity by damping of the power swings. Flexible AC transmission system (FACTS) devices are found to be very effective for this purpose. A FACTS device should have an adequate margin of variable compensation for effective damping of power swings. Therefore, while planning for FACTS controllers, the damping effect per MVar and the control cost should be taken into consideration.

II. UNIFIED POWER FLOW CONTROLLER (UPFC)

Gyugyi proposed the Unified Power Flow Controller (UPFC) concept in 1991. The UPFC was devised for the real time control and dynamic compensation of ac transmission systems, providing multifunctional flexibility required to solve many of the problems facing the delivery industry. Within the framework of traditional power transmission concepts, the UPFC is able to control, simultaneously or selectively, all the parameters affecting power flow in the transmission line (i.e., voltage, impedance and phase angle), and this unique capability is signified by the adjective “unified” in its name. Alternatively, it can independently control both the real and reactive power flows in the line.

A. Circuit Arrangement

In the presently used practical implementation, The UPFC consists of two switching converters, which in the implementations considered are voltage source inverters using gate turn-off (GTO) thyristor valves, as illustrated in the Fig.1.

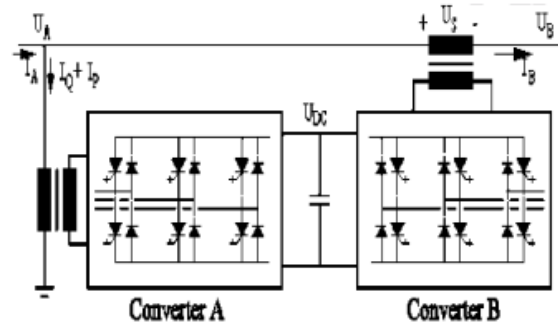


Fig.1. Basic circuit arrangement of unified power flow controller

These back to back converters labeled “Inverter 1” and “Inverter 2” in the figure, are operated from a common dc link provided by a dc storage capacitor. This arrangement functions as an ac to ac power converter in which the real power can freely flow in either direction between the ac terminals of the two inverters and each inverter can independently generate (or absorb) reactive power at its own ac output terminal.

B. Operation of UPFC

Inverter 2 provides the main function of the UPFC by injecting an ac voltage V_{pq} with controllable magnitude $V_{pq} (0 \leq V_{pq} \leq V_{pqmax})$ and phase angle $(0 \leq p \leq 360)$, at the power frequency, in series with the line via an insertion transformer. The injected voltage is considered essentially as an asynchronous voltage source. The transmission line current flows through this voltage source resulting in real and reactive power exchange between it and the ac system. The real power exchanged at the ac terminal (i.e., at the terminal of insertion transformer) is converted by the inverter into dc power that appears at the dc link as positive or negative real power demanded. The reactive power exchanged at the ac terminal is generated internally by the inverter. The basic function of inverter 1 is to supply or absorb the real power demanded by Inverter 2 at the common dc link. This dc link power is converted back to ac and coupled to the transmission line via a shunt-connected transformer. Inverter 1 can also generate or absorb controllable reactive power, if it is desired, and thereby it can provide independent shunt reactive compensation for the line. It is important to note that where as there is a closed “direct” path for the real power negotiated by the action of series voltage injection through Inverters 1 and 2 back to the line, the corresponding reactive power exchanged is supplied or absorbed locally

by inverter 2 and therefore it does not flow through the line. Thus, Inverter 1 can be operated at a unity power factor or be controlled to have a reactive power exchange with the line independently of the reactive power exchanged by the Inverter 2. This means there is no continuous reactive power flow through UPFC.

C. Basic Control Functions

Operation of the UPFC from the standpoint of conventional power transmission based on reactive shunt compensation, series compensation, and phase shifting, the UPFC can fulfill these functions and thereby meet multiple control objectives by adding the injected voltage V_{pq} , with appropriate amplitude.

Terminal Voltage Regulation, similar to that obtainable with a transformer tap-changer having infinitely small steps, as shown at (a) where $V_{pq} = V$ (boldface letters represent phasors) is injected in-phase (or anti-phase) with V_o .

relationship with respect to V_o that achieves the desired phase shift (advance or retard) without any change in magnitude.

Multifunctional Power Flow Control, executed by simultaneous terminal voltage regulation, series capacitive compensation, and phase shifting, is shown at (d) where $V_{pq} = V + V_c + V_o$.

D. Basic Principles of P and Q Control

Consider Fig. 2 At (a) a simple two machine (or two busac inter-tie) system with sending end voltage V_s , receiving end voltage V_r , and line (or tie) impedance X (assumed, for simplicity, inductive) is shown. At (b) the voltages of the system in the form of a phasor diagram are shown with transmission angle θ and $V_s \sin \theta = V_r \cos \theta = V$. At (c) the transmitted power P ($P = V^2/X \sin \theta$) and the reactive power $Q = Q_s = Q_r$ ($Q = V^2/X (1 - \cos \theta)$) supplied at the ends of the line are shown plotted against angle θ . At (d) the reactive

power $Q = Q_s = Q_r$ is shown plotted against the transmitted power corresponding to "stable values of (i.e., $0 < \theta < 90^\circ$). Basic power system of fig with the well known transmission characteristics is introduced for the purpose of providing a vehicle to establish the capability of the UPFC to control the transmitted real power P and the reactive power demands, Q_s and Q_r , at the sending end, respectively, the receiving end of the line. Consider Fig. 2. The simple power system of Fig is expanded to include the UPFC. The UPFC is represented by a controllable voltage source in series with the line which, as explained in the previous section, can generate or absorb reactive power that it, or absorbed from it, by the sending end generator. The UPFC in series with the line is represented by the phasor V_{pq} having magnitude $V_{pq} (0 \leq V_{pq} \leq V_{pqmax})$ and angle $\rho (0 \leq \rho \leq 360)$ measured from the given phase position of phasor V_s , as illustrated in the figure. The line current represented by the phasor I , flows through the

series voltage source, V_{pq} and generally results in both reactive and real power exchange. In order to represent UPFC properly, the series voltage source is stipulated to generate only the reactive power Q_{pq} it exchanges with the line. Thus the real power P_{pq} it negotiates with the line is assumed to be transferred to the sending-end generator excited. This is in arrangement with the UPFC circuit structure in which the dc link between the

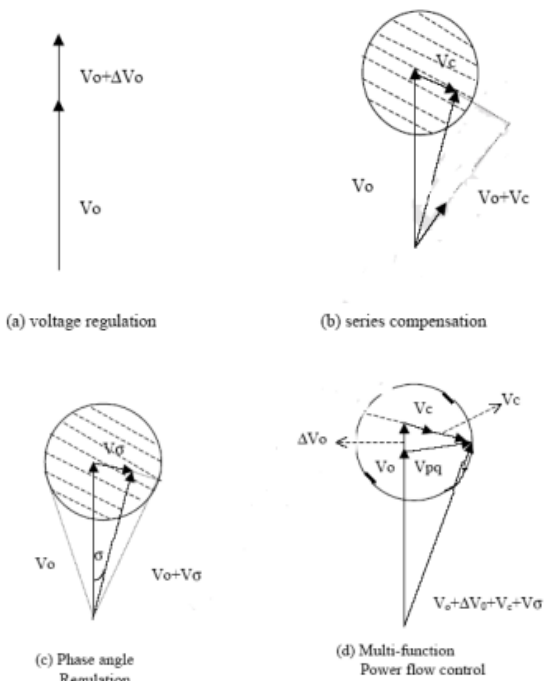


Fig. 2. Basic UPFC Control Functions: a) Voltage Regulate, b) Series Compensation, c) Angle Regulation and d) Multifunction Power.

Series capacitor compensation is shown at (b) where $V_{pq} = V_c$ is in quadrature with the line current I . Transmission angle Regulation (phase shifting) is shown at (c) where $V_{pq} = V_o$ is injected with angular

two constituent inverters establish a bi-directional coupling for real power flow between the injected series voltage source and the sending end bus.

As Fig.3 implies, in the present discussion it is further assumed for clarity that the shunt reactive compensation capability of the UPFC not utilized. This is the UPFC shunt inverter is assumed to be operated at unity power factor, its sole function being to transfer the real power demand of the series inverter to the sending-end generator. With these assumptions, the series voltage source, together with the real power coupling to the sending end generator as shown in fig.4, is an accurate representation of the basic UPFC.

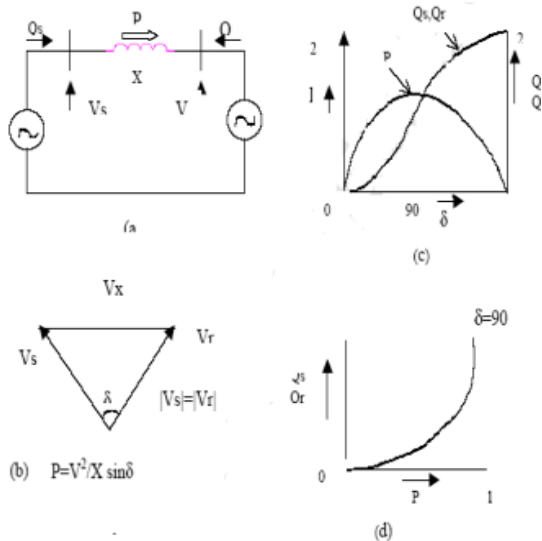


Fig.3. Simple two machine system (a) Related voltage phasor (b) Real and Reactive power versus transmission angle (c) sending end /receiving end reactive power v/transmitted real power.

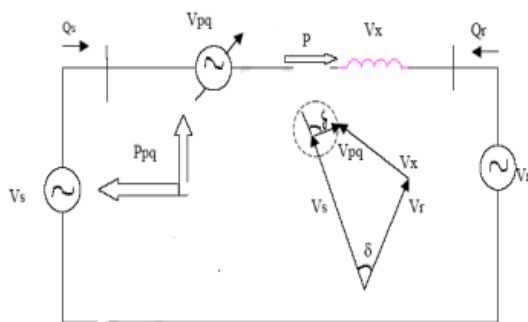


Fig.4. Two machine system with the unified power flow controller.

It can be observed in Fig that the transmission line “sees” $V_s + V_{pq}$ as the effective sending end voltage. Thus it is clear that the UPFC effects the voltage (both its magnitude and angle) across the transmission line and therefore it is reasonable to expect that it is able to control, by varying the magnitude and angle of V_{pq} , the transmittable real power as well as the reactive power demand of the line at any given transmission angle between the sending-end and receiving-end voltages.

III. MODELLING OF CASE STUDY

A. Control Strategy for UPFC

Shunt Converter Control Strategy: The shunt converter of the UPFC controls the UPFC bus voltage/shunt reactive power and the dc link capacitor voltage. In this case, the shunt converter voltage is decomposed into two components. One component is in-phase and the other in quadrature with the UPFC bus voltage. Decoupled control system has been employed to achieve simultaneous control of the UPFC bus voltage and the dc link capacitor voltage.

Series Converter Control Strategy: The series converter of the UPFC provides simultaneous control of real and reactive power flow in the transmission line. To do so, the series converter injected voltage is decomposed into two components. One component of the series injected voltage is in quadrature and the other in-phase with the UPFC bus

voltage. The quadrature injected component controls the transmission line real power flow. This strategy is similar to that of a phase shifter. The in-phase component controls the transmission line reactive power flow. This strategy is similar to that of a tap changer.

B. Basic Control System

Shunt Converter Control System: Fig.5 shows the decoupled control system for the shunt converter. The D-axis control system controls the dc link capacitor voltage and the Q-axis control system controls the UPFC bus voltage/shunt reactive power. The details of the decoupled control system design can be found. The decoupled control system has been designed based on linear control system techniques and it consists of an outer loop control system that sets the reference for the inner control system loop. The inner control system loop tracks the reference.

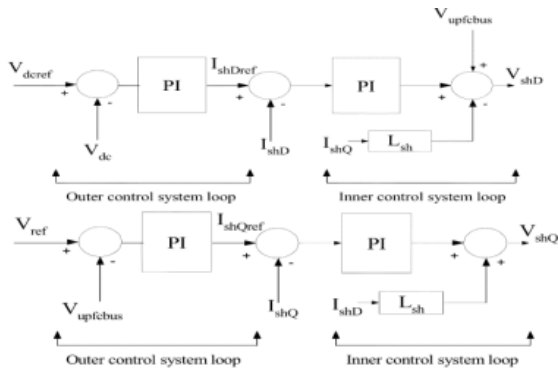


Fig.5. De-coupled D-Q axis shunt converter control system.

IV. SIMULATION RESULTS

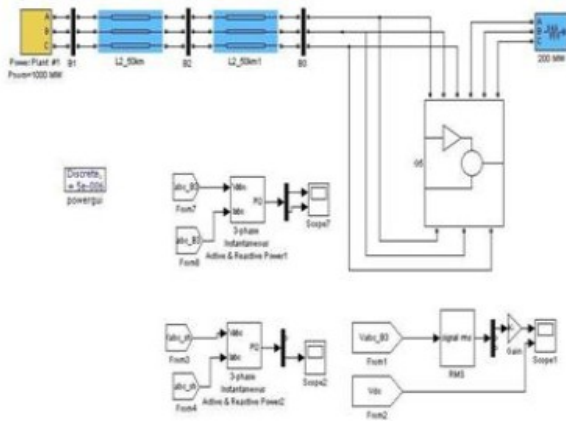


Fig.6. Model of Real and Reactive Power Coordination

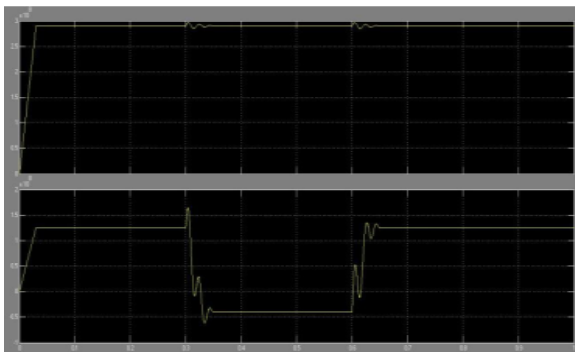


Fig.7 Simulation For Real and Reactive Power Without Coordination

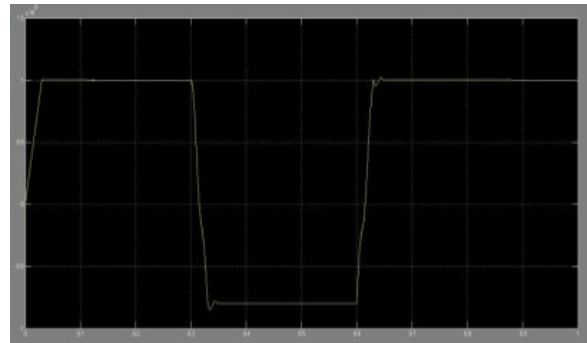


Fig.8 Simulation For Real And Reactive Power With Coordination

CONCLUSION

This paper has presented a new real and reactive power coordination controller for a UPFC. The basic control strategy is such that the shunt converter of the UPFC controls the UPFC bus voltage/shunt reactive power and the dc link capacitor voltage. The series converter controls the transmission line real and reactive power flow. The contributions of this work can be summarized as follows.

Two important coordination problems have been addressed in this paper related to UPFC control. One, the problem of real power coordination between the series and the shunt converter control system. Second, the problem of excessive UPFC bus voltage excursions during reactive power transfers requiring reactive power coordination.

Inclusion of the real power coordination controller in the UPFC control system avoids excessive dc link capacitor voltage excursions and improves its recovery during transient conditions. MATLAB simulations have been conducted to verify the improvement in dc link voltage excursions during transient conditions.

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