

# Surface Roughness Performance And Process Parameters Of Drilling Operation By Using Composite Materials

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**Abstract**\_Metal reducing is one of the maximum good sized production strategies inside the vicinity of cloth elimination. Black described metallic slicing because the elimination of metallic chips from a workpiece so as to attain a completed product with favored attributes of length, form, and surface roughness.

The imperative goal of the technological know-how of metallic slicing is the solution of realistic issues associated with the efficient and particular elimination of metal from work piece. It has been recognized that the reliable quantitative predictions of the various technological overall performance measures, preferably within the form of equations, are critical to expand optimization techniques for choosing cutting situations in method making plans.

In this thesis experiments might be performed to improve the floor end pleasant of GFRP (glass fiber reinforced polymer) composites work piece through using 8mm, 10 mm&12mm diameter HSS (M2) drill. The type is bull nose tip. The drilling parameters are velocity and feed fee for drilling of work piece GFRP. In this work, the greatest parameters of slicing velocity are 800rpm, 1000rpm and 1200rpm, feed fee are 30mm/rev, 40mm/rev and 50mm/rev and factor perspective 1200.

Taguchi method is used to look at the effect of method parameters and set up correlation among the slicing pace, feed and intensity of cut with recognize to the essential machinability issue, surface finish. Validations of the modeled equations are proved to be well in the agreement with the experimental statistics.

### **1.INTRODUCTION**

Drilling is a slicing system that uses a drill bit to reduce a hole of circular pass-phase in strong substances. The drill bit is usually a rotary slicing tool, often multipoint. The bit is pressed towards the paintings piece and turned around at fees from hundreds to lots of revolutions in keeping with minute. This forces the reducing aspect against the work piece, slicing off chips (swarf) from the hole as it's miles drilled.



In rock drilling, the hole is typically no longer made thru a circular cutting motion, though the bit is typically turned around. Instead, the hollow is normally made by hammering a drill bit into the hole with fast repeated quick moves. The hammering action may be performed from outdoor of the hole (pinnacle-hammer drill) or in the hole (down-the-hollow drill, DTH). Drills used for horizontal drilling are called drifter drills.

In uncommon instances, in particular-shaped bits are used to cut holes of non-circular



esegm ent; a recta ngul ar cross segm ent is possi ble.

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#### Process

Bored openings are portrayed by their sharp edge on the passage side and the nearness of burrs on the leave side (except if they have been evacuated). Additionally, within the gap more often than not has helical feed marks.

Penetrating may influence the mechanical properties of the workpiece by making low remaining worries around the gap opening and a flimsy layer of exceedingly focused and aggravated material on the recently framed surface. This makes the workpiece become increasingly helpless to consumption and split proliferation at the focused on surface. A completion task might be done to maintain a strategic distance from these hindering conditions.

For fluted boring apparatus, any chips are evacuated by means of the flutes. Chips may shape long spirals (undesirable)or little drops, contingent upon the material, and procedure parameters. The sort of chips framed can be a pointer of the machinability of the material, with long chips proposing poor material machinability.

At the point when conceivable bored openings ought to be found opposite to the workpiece surface. This limits the boring apparatus' inclination to "walk", that is, to be redirected from the proposed focus line of the drag, making the gap be lost. The higher the length-to-measurement proportion of the boring tool, the more prominent



the propensity to walk. The inclination to walk is likewise acquired in different ways, which include: Building up a focusing imprint or highlight before penetrating, for example, by: Throwing, embellishment, or producing an imprint into the work piece

### 2.LITERATURE REVIEW

P. Rahme et.al [1] had been considered systematic model was created to decide the basic push power at delamination at the gap exit. This model gives the penetrating push power as an element of the cutting conditions. At last, the two considered models are utilized to decide the ideal cutting conditions for without delamination penetrating. The outcomes are approved numerically and tentatively. A boring push power model is created so as to compute the penetrating powers of each zone in capacity of the feed rate per tooth. The consequences of the two proposed models are utilized to compute the basic feed rate per tooth, at delamination, on account of an enormous distance across bend drill, without diminishing its etch edge. These feed rates are resolved for the two zones of the drill. They are determined by the quantity of the non-bored handles staying under the drill. The most basic feed rate per tooth compares to the least worth.

Tom Sunny et.al [2] had been considered the impact of speed and feed on delamination conduct of composite materials by leading boring investigations utilizing Taguchi's L25, 5-level symmetrical exhibit and Analysis of fluctuation by utilizing three unique instruments in particular Twist drill, End plant and Kevlar drill. ANOVA was utilized to examine the information got from the examinations lastly decide the ideal penetrating parameters in boring Glass fiber strengthened composite (GFRP) materials. Consequences of these analyses uncovered that expanding the shaft speed and diminishing feed rate can lessen the delamination inside cutoff points of determined speed and feed rates. Too low feed rate and too high axle speed can likewise build the delamination. Results additionally uncovered that feed rate is the more persuasive factor on delamination than shaft speed.

Patil A.A [3] had done audit on penetrating on composite material, It has been anticipated that the greater part of the issue related with gap making task, for example, boring, can be ascribed to the power produced during cutting activity. Numerous advancements and tests are continuing boring of Sandwich composite for harm free boring alongside the nature of the gap and the impact of hardware geometry and apparatus material. This paper goes for the exhaustive expository and test examination work done on the composites material.

R.A. Kishore et al.[4] Studied the impact of the cutting pace, the feed rate, and the drill point geometry on the remaining elasticity of the bored unidirectional glass fiber fortified epoxy composite utilizing the Taguchi technique and recommends the ideal conditions for greatest lingering rigidity. Three significant parameters, that is the drill point geometry, the cutting velocity and the feed rate have been contemplated. The



ideal degrees of the drill point geometry, the cutting pace and the feed rate have been built up for getting most extreme leftover rigidity in penetrated UDGFRP covers. The greatest leftover quality is found with 8-aspect drill at cutting rate of 750 rpm and feed pace of 15 mm/min. It is seen that the penetrating incited harm at higher cutting rates seriously influences the lingering rigidity of bored overlays. The ideal choice of the drill point geometry is additionally imperative to discover the base boring instigated harm and in this manner the most extreme lingering rigidity.

C. C. Tsao [5] Analyzed the Taguchi technique for boring quality partners with center drill. The push power and surface unpleasantness of center drill with drill parameters (coarseness size of precious stone, thickness, feed rate and axle speed) in boring Carbon Fiber Reinforcement Plastic (CFRP) covers was tentatively researched. Composite material for penetrating was created utilizing autoclave forming. A L27 symmetrical exhibit and sign to-commotion (S/N) were utilized to examine the impact of drill parameters. Utilizing Taguchi strategy for plan of a strong examination the association among components is additionally researched. For push power, thickness and feed rate are the most noteworthy elements and for surface harshness, the feed rate and axle speed are the most critical factors in penetrating GFRP covers as tentatively and scientifically acquired. When all is said in done fast and low penetrating feed rate are prescribed for the creation of delamination free and great surface completion gaps in epoxy composites.

### **3.METHODOLOGY**

Taguchi Method is advanced with the aid of Dr. Genichi Taguchi, a Japanese quality management consultant. The method explores the idea of quadratic excellent loss characteristic and makes use of a statistical measure of overall performance referred to as Signal-toNoise (S/N) ratio. The S/N ratio takes each the mean and the variability into consideration. The S/N ratio is the ratio of the imply (Signal) to the standard deviation (Noise). The ratio depends at the satisfactory traits of the product/technique to be optimized. The popular S/N ratios typically used are as follows: - Nominal is Best (NB), Lower the Better (LB) and Higher the Better (HB).

#### **3.1 Input parameters and their stages**

| PROCESS           | LE   | LEVEL2 | LEVEL3 |
|-------------------|------|--------|--------|
| PARAMETERS        | VEL1 |        |        |
| SPEED(rpm)        | 1200 | 1000   | 800    |
| DRILL BIT DIA(mm) | 8    | 10     | 12     |
| Feed (rev/min)    | 30   | 40     | 50     |

Selected enter Parameters



### **3.2 OBJECTIVE**

The principle objective in structure of test is to contemplate the connection between the reaction and factors. Structure of trial is a technique to limit the quantity of tests so as to arrive at ideal conditions. To investigate the connection between the reaction and the free factors, the information required are acquired tentatively. To diminish the quantity of analyses, the quantity of information was kept at least. In this work, 9 tests dependent on full factorial structure of the analyses utilizing three-level cutting parameters and three-level edge focuses are given in Table 2. The parameter levels are picked dependent on the essential tests.

### 4.EXPERIMENTAL INVESTIGATION

The experiments are done on the drilling machine with the following parameters:

WORK PIECE MATERIAL – GFRP (glass fiber reinforced polymer)

DRILL BIT DIA-8mm, 10 mm, 12mm

CUTTING SPEED - 1200rpm, 1000rpm, 800rpm,

Feed-30mm/min,40 mm/min,50 mm/min.

### **EXPERIMENTAL PHOTOS**





**Drilling process** 



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### **Final component**

## **4.1 INPUT PARAMETERS**

| PROCESS           | LE   | LEVEL2 | LEVEL3 |
|-------------------|------|--------|--------|
| PARAMETERS        | VEL1 |        |        |
| SPEED(rpm)        | 1200 | 1000   | 800    |
| DRILL BIT DIA(mm) | 8    | 10     | 12     |
| Feed (rev/min)    | 30   | 40     | 50     |



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| JOB NO. | SPEED (rpm) | DRILL BIT DIA(mm) | FEED<br>(Rev/min) |
|---------|-------------|-------------------|-------------------|
| 1       | 1200        | 8                 | 30                |
| 2       | 1200        | 10                | 40                |
| 3       | 1200        | 12                | 50                |
| 4       | 1000        | 8                 | 40                |
| 5       | 1000        | 10                | 50                |
| 6       | 1000        | 12                | 30                |
| 7       | 800         | 8                 | 50                |
| 8       | 800         | 10                | 30                |
| 9       | 800         | 12                | 40                |

### **4.2 SURFACE FINISH VALUES**

|         |             | DRILL BIT | FEED      | Surface finish     |
|---------|-------------|-----------|-----------|--------------------|
| JOB NO. | SPEED (rpm) |           | (Rev/min) | $(\mathbf{R}_{a})$ |
|         |             | DIA(mm)   |           | μm                 |
|         |             |           |           |                    |
| 1       | 1200        | 8         | 30        | 2.56               |
| 2       | 1200        | 10        | 40        | 2.24               |
| 3       | 1200        | 12        | 50        | 1.86               |
| 4       | 1000        | 8         | 40        | 2.97               |
| 5       | 1000        | 10        | 50        | 3.21               |
| 6       | 1000        | 12        | 30        | 3.14               |
| 7       | 800         | 8         | 50        | 3.56               |
| 8       | 800         | 10        | 30        | 4.52               |
| 9       | 800         | 12        | 40        | 3.86               |



#### 5.0PTIMIZATION OF SURFACE FINISH USING MINITAB SOFTWARE

#### **5.1 Design of Orthogonal Array**

First Taguchi Orthogonal Array is designed in Minitab17 to calculate S/N ratio and

Means which steps is given below:

| 🗐 S                                  | ession                 |                         |                          |                          |                       |           |           |           |           |         |     |     |     |     |     |     |     |     |     |     |             |
|--------------------------------------|------------------------|-------------------------|--------------------------|--------------------------|-----------------------|-----------|-----------|-----------|-----------|---------|-----|-----|-----|-----|-----|-----|-----|-----|-----|-----|-------------|
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| Th                                   | is Softwa<br>mmercial  | use of th               | irchased i<br>le Softwar | for acader<br>re is prob | nic use o<br>hibited. | nly.      |           |           |           |         |     |     |     |     |     |     |     |     |     |     |             |
| 1                                    |                        |                         |                          |                          |                       |           |           |           |           |         |     |     |     |     |     |     |     |     |     |     |             |
|                                      |                        |                         |                          |                          |                       |           |           |           |           |         |     |     |     |     |     |     |     |     |     |     |             |
| •                                    |                        |                         |                          |                          |                       |           |           |           |           |         |     |     |     |     |     |     |     |     |     |     | •           |
|                                      |                        |                         |                          |                          |                       |           |           |           |           |         |     |     |     |     |     |     |     |     |     |     |             |
| (11 w                                | orksheet 1 *           | ***                     |                          |                          |                       |           |           |           |           |         |     |     |     |     |     |     |     |     |     |     |             |
|                                      | orksheet 1 *<br>C1     | <br>C2                  | C3                       | C4                       | C5                    | C6        | C7        | C8        | C9        | C10     | C11 | C12 | C13 | C14 | C15 | C16 | C17 | C18 | C19 | C20 | ια Σ<br>C21 |
| •<br>•                               | orksheet 1 *<br>C1     | C2                      | C3                       | C4                       | C5                    | C6        | C7        | C8        | C9        | C10     | C11 | C12 | C13 | C14 | C15 | C16 | C17 | C18 | C19 | C20 | ο Σ<br>C21  |
| •<br>•<br>1<br>2                     | orksheet 1 *<br>C1     | C2                      | C3                       | C4                       | C5                    | C6        | C7        | C8        | C9        | C10     | C11 | C12 | C13 | C14 | C15 | C16 | C17 | C18 | C19 | C20 | C21         |
| 1<br>2<br>3                          | 'orksheet 1 *<br>C1    | C2                      | C3                       | C4                       | C5                    | C6        | C7        | C8        | C9        | C10     | C11 | C12 | C13 | C14 | C15 | C16 | C17 | C18 | C19 | C20 | α Σ<br>C21  |
| • W                                  | C1                     | C2                      | C3                       | C4                       | C5                    | C6        | C7        | C8        | C9        | C10     | C11 | C12 | C13 | C14 | C15 | C16 | C17 | C18 | C19 | C20 | C21         |
| 1<br>2<br>3<br>4<br>5                | C1                     | C2                      | C3                       | C4                       | C5                    | C6        | C7        | C8        | C9        | C10     | C11 | C12 | C13 | C14 | C15 | C16 | C17 | C18 | C19 | C20 | ε Σ<br>C21  |
| 1<br>2<br>3<br>4<br>5<br>6<br>7      | C1                     | C2                      | C3                       | C4                       | C5                    | C6        | C7        | C8        | C9        | C10     | C11 | C12 | C13 | C14 | C15 | C16 | C17 | C18 | C19 | C20 | C21         |
| 1<br>2<br>3<br>4<br>5<br>6<br>7<br>8 | C1                     | C2                      | 3                        | C4                       | C                     | C6        | C7        | C8        | C9        | C10     | C11 | C12 | C13 | C14 | C15 | C16 | C17 | C18 | C19 | C20 | C21         |

### FACTORS

| A         SPEED         1200 1000 800         1         I <thi< th=""> <thi< th=""> <thi< th=""></thi<></thi<></thi<> | Fact I | Name     | Level Values  | Colum | In | Leve |
|---|--------|----------|---------------|-------|----|------|
| B         DRILL BIT         8 10 12         2          3         3         3           C         FEED         30 40 50         3          3          3  | A SP   | PEED     | 1200 1000 800 | 1     | •  | 3    |
| C FEED 30 40 50 3 💌 3   | B DF   | RILL BIT | 8 10 12       | 2     | •  | 3    |
|   | C FE   | EED      | 30 40 50      | 3     | •  | 3    |
|   |        |          |               |       |    |      |



| Taguchi Design   |   |                                       | ×       |
|--|---|---------------------------------------|---------|
| Type of Design<br>C 2-Level Design<br>G 3-Level Design<br>C 4-Level Design<br>C 5-Level Design<br>C Mixed Level Design | (2 to 31 factor<br>(2 to 13 factor<br>(2 to 5 factors<br>(2 to 6 factors<br>(2 to 26 factor | rs)<br>rs)<br>;)<br>;)<br>rs)         |         |
| Number of factors: 3   | •   | Display Availal<br>Designs<br>Options | Factors |
| Help   |   | ОК                                    | Cancel  |

#### **OPTIMIZATION OF PARAMETERS**

| 🖽 Wo | Worksheet 1 *** |               |      |  |  |  |  |  |  |
|------|-----------------|---------------|------|--|--|--|--|--|--|
| Ŧ    | C1              | C2            | C3   |  |  |  |  |  |  |
|      | SPEED           | DRILL BIT DIA | FEED |  |  |  |  |  |  |
| 1    | 1200            | 8             | 30   |  |  |  |  |  |  |
| 2    | 1200            | 10            | 40   |  |  |  |  |  |  |
| 3    | 1200            | 12            | 50   |  |  |  |  |  |  |
| 4    | 1000            | 8             | 40   |  |  |  |  |  |  |
| 5    | 1000            | 10            | 50   |  |  |  |  |  |  |
| 6    | 1000            | 12            | 30   |  |  |  |  |  |  |
| 7    | 800             | 8             | 50   |  |  |  |  |  |  |
| 8    | 800             | 10            | 30   |  |  |  |  |  |  |
| 9    | 800             | 12            | 40   |  |  |  |  |  |  |

### Analyze Taguchi Design – Select Responses

| C4<br>C5 | SURFACE ROUGHNES<br>SURAFCE ROUGHNES | Response data are         | in:<br>INESS'-'SURAFCE | ROUGHNESS 1      |
|----------|--------------------------------------|---------------------------|------------------------|------------------|
|          |                                      |                           |                        |                  |
|          |                                      | Graphs                    | Analysis               | Terms            |
|          | Select                               | Graphs<br>Analysis Graphs | Analysis<br>Options    | Terms<br>Storage |



Terms

| Analyze Taguchi Desig                            | n: Terms      | ×   |
|--|---------------|---|
| Available Terms:<br>AB<br>AC<br>BC               | ><br>>><br><< | Selected Terms:<br>A:SPEED<br>B:DRILL BIT DIA<br>C:FEED |
| Factors:<br>A:SPEED<br>B:DRILL BIT DIA<br>C:FEED |               |   |
| Help   | ОК            | Cancel  |



S/N ratio plot





Means plot

# 5.5 Results

Taguchi strategy focuses on the significance of examining the reaction variety utilizing the sign to-clamor (S/N) proportion, bringing about minimization of value trademark variety because of wild parameter. The cutting power is considered as the quality trademark with the idea of "the bigger the-better". The S/N proportion for the bigger the-better is:

### $S/N = -10 * log(\Sigma(Y2)/n))$

Where n is the quantity of estimations in a preliminary/push, for this situation, n=1 and y is the deliberate an incentive in a run/push. The S/N proportion esteems are determined by mulling over above Eqn. with the assistance of programming Minitab 17.

#### Investigation and Discussion

Despite the class of the exhibition attributes, a more prominent S/N worth compares to a superior execution. Along these lines, the ideal degree of the machining parameters is the level with the best worth.

Axle Speed: - The impact of parameters axle speed superficially completion is appeared above figure for S/N proportion. So the ideal axle speed is 1200 rpm.

Feed Rate: - The impact of parameters feed rate superficially completion is appeared above figure S/N proportion. So the ideal feed 50 mm/rev.



#### **6.CONCLUSION**

In this proposal an endeavor to utilize Taguchi advancement strategy to advance penetrating parameters during work piece material durlene fiber. The penetrating parameters are speed and feed rate for boring of work piece durlene fiber. In this work, the ideal parameters of cutting pace are 800rpm, 1000rpm and 1200rpm, feed rate are 30mm/rev, 40mm/rev and 50mm/rev and point edge 1200. Exploratory work is directed by thinking about the above parameters. surface completion esteems are approved tentatively.

By watching the exploratory outcomes and by taguchi, the accompanying ends can be made: To show signs of improvement surface completion, the ideal parameters are speed – 1200rpm, feed–50mm/rev.

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