

A 400 μ W 3rd Order LPF with -5 to 27dB Variable Gain for 3G Direct Conversion Receiver in 180nm CMOS Technology

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Abstract

Design of an ultra low power channel select filter with variable gain for the direct conversion wireless 3G receiver is proposed. Portable wireless communication receiver requires a highly linear and low noise base band filter to achieve good sensitivity. Low power consumption is desirable for Portable systems. The proposed 3rd order continues time low pass filter consists of a pre passive filtering stage followed by an OPAMP stage. The pre passive filtering section with minimum number of resistors and capacitors provides high out band linearity and good spurious free dynamic range (SFDR) of the receiver. The single OPAMP stage provides four pole transfer function and reduces in band noise by the use of Cascode structure. Finally, inclusion of a variable gain stage, improves the system suitability for the practical applications. The simulated results of the proposed filter show 12 dBm of Input referred 3rd order intercept point (IIP3), 33 dBm of out of band IIP3, with 2.5MHz 3dB frequency. The circuit shows -5 to 27dB variable gain by consuming 400 μ W power from 1.8V supply in 180nm CMOS.

Key words: Direct Conversion Receiver (DCR); Low Pass Filter (LPF); Unity Gain Bandwidth (UGB); Out of Band IIP3; In Band IIP3; Common Mode Feedback (CMFB)

INTRODUCTION

The RF signal that is received in direct conversion receiver is first filtered and amplified with a pre-select band pass filter and Low Noise Amplifier respectively. Fortunately, no external channel select filter is required and the base band filter section is responsible for filtering and selecting the desired channel in 3G RF spectrum. The selectivity and linearity requirements of base band filter are more critical than in any other architectures due to the absence of preceding highly linear high Q RF and IF filters. Many papers have been published making new

proposals for the design of these filters and each concentrate on getting high linearity and selectivity. Many topologies have been proposed to design filter such as G_m -C, active-RC, and Integrated active filters. Design of Op-Amp and trans-conductor is crucial in design of these active filters which are the basic building blocks of analog circuits.

Mohammad Abdulaziz, Markus Tormanen, Henrik Sjolund proposed a fourth order Butterworth low pass filter with 10MHz frequency is implemented in 65nm CMOS draws a current of 3.5mA from 1.2V supply and this

occupies an area nearly 0.19mm². It consumes power of 4.2mW [1].

Yong Chen, Pui-in Mak, Li Zhang, He Qian and Yan Wang proposed filter which is designed using LC elements of fifth order is having 20MHz cut-off frequency. It consists of transistorized LC ladder elements realized by combining source followers with Q enhanced floating differential active inductors [2].

Tien-Yu Lo, Chi-Hsiang [3] proposed a novel four pole filter has been implemented of which two poles are provided by Op-Amp to handle the blockers with a supply of 1V. The four pole filter topology includes an Op-Amp which is given a pole tracking ability to achieve low in band levels, high out of band linearity and low power consumption. Although the power consumption and area occupied are less compared to [1] and [2], there is a significant loss between the input and output signal nearly 10-12dB.

Many filters have been designed but most of them are limited with various trade-offs between power consumption, area occupied on the chip etc. [4]-[15]

The proposed circuit gives Op-Amp an additional capability so that the loss is compensated. A variable gain stage is added to the Op-Amp as the final stage so that not only compensating the loss, the signal can be filtered and boosted. The design of filter is a 4th order transfer function in which two poles are given by the passive stage and remaining is obtained from the Op-Amp that works with a power supply of 1.8V. High in-band and out band linearity is obtained along with low power consumption.

FILTER IMPLEMENTATION

Generally, active RC filter designs require large gain and bandwidth. In order to obtain higher order transfer function, a cascade of bi-quads is to be implemented which require high power. In order to reduce the power consumption, Op-Amp is given pole tracking ability so that two of four poles are obtained through Op-Amp and remaining two from the passive stage of the filter. Op-Amp is designed such that its gain is varied such that the loss occurring up to its preceding stage is compensated so that signal is filtered as well as boosted. The overall design of the proposed filter circuit is given in Fig.1.

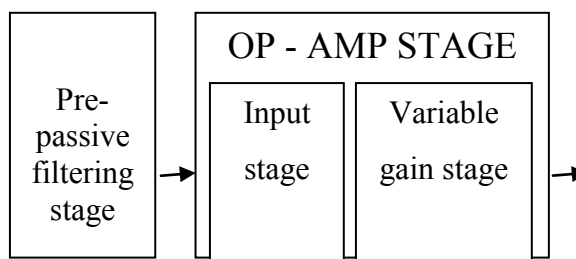


Fig.1 Block diagram of 3rd order LPF

Passive stage contains differential RC sections which contribute two poles in overall four pole filter transfer function. This passive stage acts like a pre- filtering stage hence that the signal is conditioned before entering into the Op-Amp circuit such that the noise of Op-Amp will not get added to the external noise so the amplification of noise will be significantly decreased. The circuit of the passive section is shown in Fig.2.

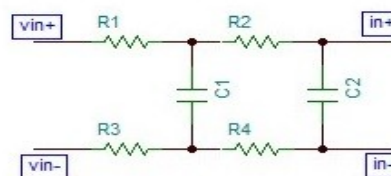


Fig.2 Pre - Passive filtering stage of LPF circuit

OPAMP IMPLEMENTATION

For the proposed filter circuit in this paper, the op amp should be able to satisfy two aspects. It should be able to provide two poles out of four poles of the complete transfer function of the circuit and the other is the ability to vary its overall gain such that no loss has to be obtained in the signal between input and output. The Op-Amp circuit has a bias generation stage, input stage, and a variable gain stage as a final stage.

For the bias generation stage, constant-Gm bias stage is used in order to generate the bias voltages for the input stage. The poles of the Op-Amp are obtained in the input stage which has capacitors C_1 and C_2 . Degenerated trans-conductance of the transistors M_1 and M_2 and Capacitance C_2 provides the necessary UGB. The other pole frequency is obtained by the trans-conductance of pair of cascoded transistors and capacitor C_1 . So the DC gain of the Op-Amp is degenerated trans-conductance of the Op-Amp multiplied by the impedance seen from the Op-Amp output. Overall open loop transfer function of Op-Amp is

$$\frac{V_{out}}{V_{in}} = \frac{G_m}{sC_2} \left(\frac{R_0}{sC_1} + 1 \right) \quad (1)$$

Where R_0 is the output impedance of input stage of Op-Amp, G_m is the degenerated trans-conductance of the transistors M_1 and M_2 . Here, pole frequency formed by C_2 is the dominant pole in the transfer function of Op-Amp. Since, Op-Amp provides a 2nd order transfer function, phase response of Op-Amp should be taken care so that significant margin has to be maintained so that phase response of Op-Amp does not reach

180°. As the phase margin depends on the non-dominant pole of the system, certain value of C_1 is selected such that good amount of margin in phase is maintained.

A constant g_m bias is used so that, the process variations do not change the bias voltages hence, accurate response is maintained. Instead of using the error amplifier in common mode feedback circuit, it is simplified by using simple resistive CMFB circuit in order to optimize the power consumption.

The final stage of the Op-Amp circuit is the variable gain stage which is responsible for compensating the signal loss. This stage is composed of differential PMOS common source amplifier stage which gives op-amp a variable gain capability so that it boosts the signal to the required level. The minimum value of R is taken as 1K and maximum value is taken as 50K in this design. Improved in-band and out-band IIP3 can be obtained using this variable gain stage of Op-Amp. The overall filter circuit is shown in Fig.3.

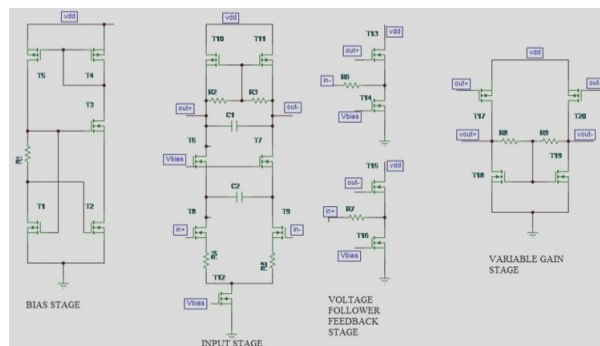
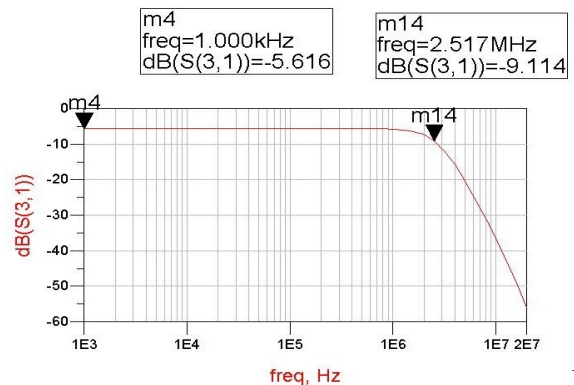


Fig. 3 Op-Amp Schematic

SIMULATION RESULTS

The proposed filter is fabricated in 180nm CMOS technology using a supply voltage of 1.8V. The magnitude at frequencies 3.162MHz

and 31.62MHz are observed as -11.895dBm and -70.238dBm respectively showing the 3 pole roll off in in-band. S21plots are simulated for minimum gain and maximum gain. The minimum value observed as -5.616dB DC gain whose 3dB gain is -9.114dB at 2.5MHz. The maximum gain observed as 27.621dB as DC gain and 3dB gain is 24.108dB at 2.5MHz as shown in Fig.4 and Fig.5 respectively. s21 response for different R values of variable gain stage is shown in Fig.6 which offers a minimum gain of -5.616dB and maximum gain of 27.621dB. Maximum current consumption is observed as 225.57μA is shown in Fig.7. Thus maximum power consumption is 406.026μW with a power supply of 1.8V which is reasonable even the signal is boosted.



Fig

. 5 S21 plot for minimum gain

The circuit is subjected to two tone inter modulation test with both in band and out band signals for both minimum and maximum gain. Two -30dBm signals are applied at 1MHz and 1.1MHz for which an in-band IIP3 of 15.663dBm is observed at maximum gain and 23.087dBm of in band IIP3 at minimum gain which shows the better linearity even offering the gain. Plots corresponding to the above analysis are given in Fig.8 and Fig.9. Two -30dBm signals are applied at 10MHz and 21MHz for which out band IIP3 of 46.509dBm is obtained for minimum gain and 34.359dBm for maximum gain giving the best linearity performance for the given test signals.

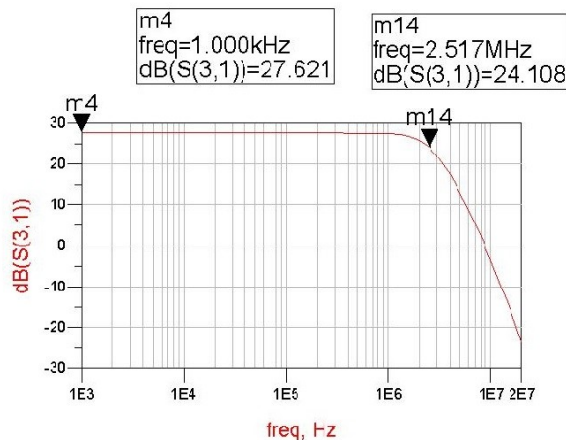


Fig. 4 S21 plot for maximum gain

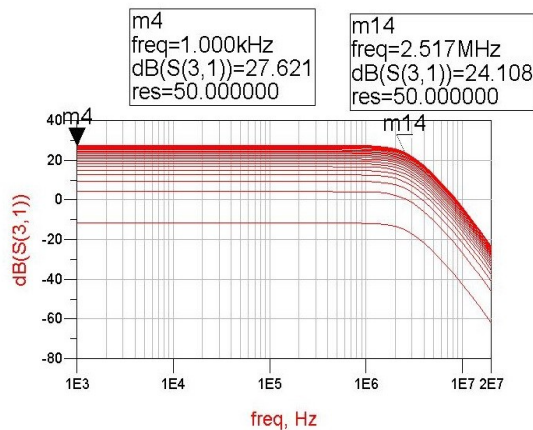


Fig.6. S21 plot for different values of R in variable gain stage

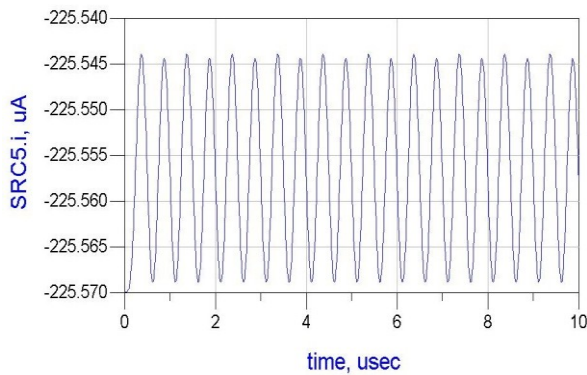


Fig. 7 Transient current plot

Plots corresponding to the above analysis are given in Fig.10 and Fig.11. The overall power consumption of the circuit including the whole Op-Amp is $406.026\mu\text{W}$.

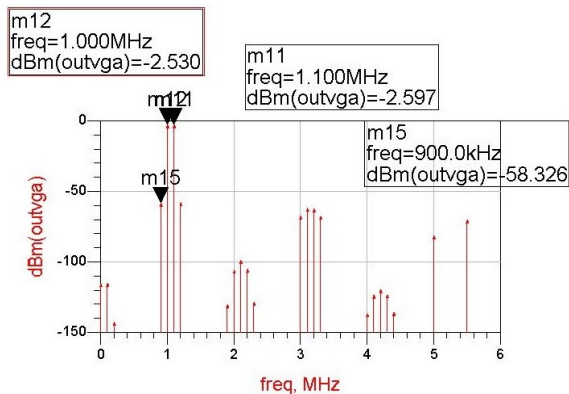


Fig. 8 In – band IIP3 for maximum gain

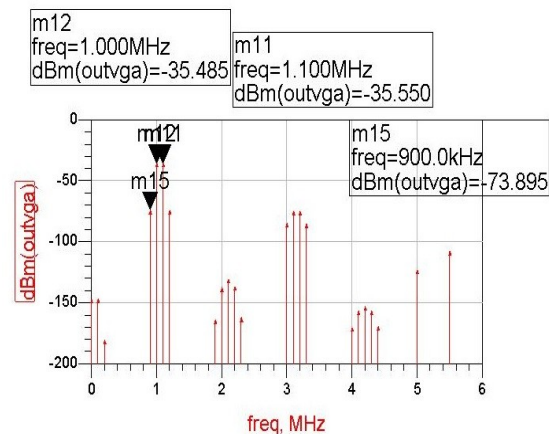


Fig. 9 In – band IIP3 for minimum gain

Noise analysis has been done and the plot of the noise spectrum is mentioned in Fig.12. It is observed that there is an input referred in-channel noise of $13.25\mu\text{V}$ i.e. -97.555dBV .

From the two tone inter-modulation test results, it is observed that

$$\text{In-band IIP3} = 23.087\text{dBm}$$

$$\text{Out-of-band IIP3} = 46.509\text{dBm}$$

In-band SFDR is found to be 71.755dBV and out-of-band SFDR is found to be 83.37dBV .

Table.1 Performance Summary of 3rd order LPF

Parameter	Simulated Result
CMOS technology process	180nm
Cut-off frequency	2.5MHz
In – Band IIP3 for minimum gain	-23.087dBm
In – Band IIP3 for maximum gain	15.663dBm
Out – of – Band IIP3 for minimum gain	46.509dBm
Out – of – Band IIP3 for maximum gain	34.359dBm
Out – of – Band SFDR	87.37dBV
In – band SFDR	71.755dBV
FoM (Out – of – Band)	1.147×10^{-3} fJ
FoM (In – Band)	4.17×10^{-2} fJ
Power consumption	$405.981\mu\text{W}$

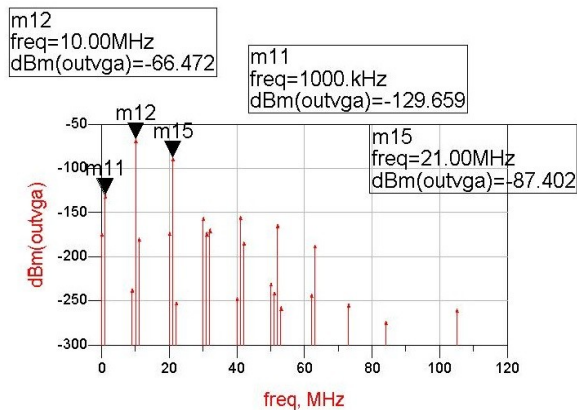


Fig.10 Out – of – band IIP3 for maximum gain

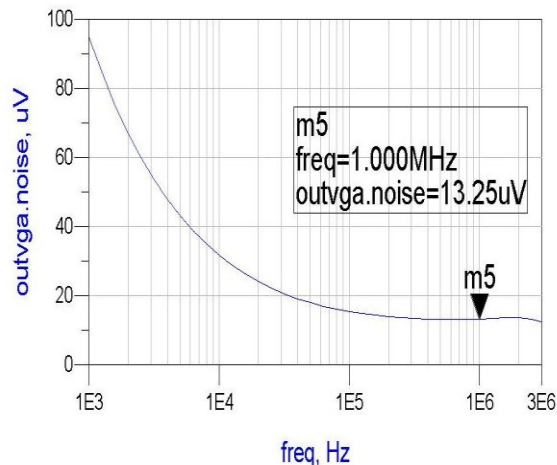
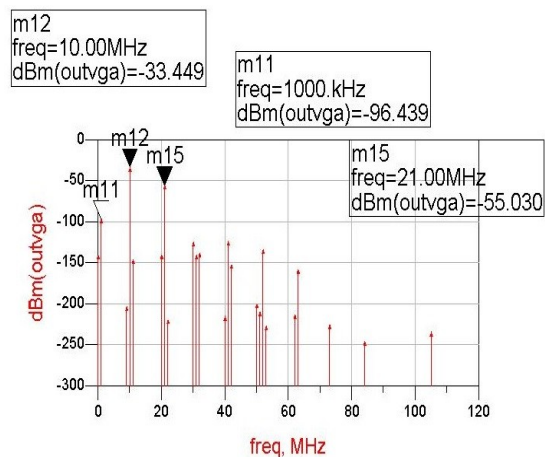


Fig.12 Input referred in-channel noise spectrum



11. Out – of – band IIP3 for minimum gain

Fig.

The figure of merits (FoM) for in-band and out-of-band are found to be

$$\text{FoM (out-of-band)} = 1.147 \times 10^{-3} \text{ fJ}$$

$$\text{FoM (In-band)} = 4.17 \times 10^{-2} \text{ fJ}$$

The performance summary of the design is mentioned in Table.1.

CONCLUSION

The present study of the proposed research work is design and implementation of 3rd order Butterworth Low Pass Filter is successfully completed with variable gain capability of -5dB to 27dB. The cut-off frequency of the channel selection filter is set to 2.5MHz which makes it suitable for 3G radio frequency specifications. This filter achieves better linearity even at a high gain operation of Op-Amp which is implemented.

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Circuit

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