

International Journal of Research (IJR) e-ISSN: 2348-6848, p- ISSN: 2348-795X Volume 3, Issue 01, January 2016 Available at http://internationaljournalofresearch.org

Cascaded Two-Level Inverter using Fuzzy logic Based multilevel STATCOM for High –Power Applications

S.Satya Sri¹ & K.Kranthi Pratap Singh²

¹M.Tech Scholar, Dept of EEE, A.S.R College of Engineering and Technology, JNTUK, A.P ²Assistant Professor, Dept of EEE, A.S.R College of Engineering and Technology, JNTUK, A.P

Abstract:—

Multilevel inverters have received more attentions their considerable advantages such as high power quality, lower harmonic components, better electromagnetic consistence, lower dv/dt and lower switching losses. Lot of research was going on multi level inverter topologies and many researchers are proposed so many multi level inverter topologies. In this paper, a simple static var compensating scheme using a cascaded two-level inverter-based multilevel inverter is proposed. The topology consists of two standard two-level inverters connected in cascade through open-end windings of a three-phase transformer. The dc-link voltages of the inverters are regulated at different levels to obtain four-level operation. The simulation study is carried out in MATLAB/SIMULINK to predict the performance of the proposed scheme under balanced and unbalanced supply-voltage conditions.

Keywords: DC-link voltage balance; multilevel inverter; power quality (PQ); static compensator (STATCOM)

I. INTRODUCTION

The application of (FACTS) controllers, such flexible ac transmission systems static as compensator (STATCOM) and static synchronous series compensator (SSSC), is increasing in power systems. This is due to their ability to stabilize the transmission systems and to improve power quality (PQ) in distribution systems. STATCOM is popularly accepted as a reliable reactive power controller replacing conventional var compensators, such as the thyristor-switched capacitor (TSC) and thyristorcontrolled reactor (TCR). This device provides compensation, reactive power active power oscillation damping, flicker attenuation, voltage regulation, etc...

Generally, in high-power applications, var compensation is achieved using multilevel inverters

[2]. These inverters consist of a large number of dc sources which are usually realized by capacitors. Hence, the converters draw a small amount of active power to maintain dc voltage of capacitors and to compensate the losses in the converter. However, due to mismatch in conduction and switching losses of the switching devices, the capacitors voltages are unbalanced. Balancing these voltages is a major research challenge in multilevel inverters. Various control schemes using different topologies are reported in [3]-[7]. Among the three conventional multilevel inverter topologies cascade H-bridge is the most popular for static var compensation [5], [6]. However, the aforementioned topology requires a large number of dc capacitors. The control of individual dc-link voltage of the capacitors is difficult.

Each bidirectional power switch includes two IGBTs, two power diodes, and one driver circuit if the common emitter configuration is used. Therefore, in these topologies, the installation space and total cost of the inverter increase. As a result, several asymmetric cascaded multilevel inverters have been presented in which the unidirectional switches from the voltage point of view and the bidirectional switches from the current point of view are used in them. Each unidirectional switch consists of an IGBT with an anti parallel diode. Two of these topologies have been presented in [20]. Two other algorithms for the H-bridge cascaded multilevel inverter have been also presented in [9] and [10]. Because of the and used unidirectional asymmetric topology switches, it seems that the lower number of power electronic devices is the main advantage of these inverters. However, the main disadvantage of the asymmetric topologies is the lost of modularity,



e-ISSN: 2348-6848, p- ISSN: 2348-795X Volume 3, Issue 01, January 2016 Available at http://internationaljournalofresearch.org

which means the use of a high variety of semiconductor devices and dc voltage sources.

Various var compensation schemes based on this topology are reported in [8]–[10]. In [9], a three-level inverter and two level inverter are connected on either side of the transformer low-voltage winding. The dc-link voltages are maintained by separate converters. In [10], three-level operation is obtained by using standard two-level inverters. The dc-link voltage balance between the inverters is affected by the reactive power supplied to the grid.

II. PROPOSED TOPOLOGY- CASCADED TWO-LEVEL INVERTER-BASED MULTILEVEL STATCOM

Fig. 1 shows the power system model considered in this paper [10]. Fig. 2 shows the circuit topology of the cascaded two-level inverterbased multilevel STATCOM using standard twolevel inverters. The inverters are connected on the low-voltage (LV) side of the transformer and the high-voltage (HV) side is connected to the grid. The dc-link voltages of the inverters are maintained constant and modulation indices are controlled to achieve the required objective. The proposed control scheme is derived from the ac side of the equivalent circuit which is shown in Fig. 3. In the figure, and are the source voltages referred to LV side of the transformer, and are the resistances which represent the losses in the transformer and two inverters, and are leakage inductances of transformer windings, and and are the output voltages of inverters 1 and 2, respectively. are the leakage resistances of dc-link capacitors and , respectively. Assuming and applying KVL on the ac side, the dynamic model can be derived using [10] as

$$\begin{bmatrix} \frac{di'_a}{dt} \\ \frac{di_b}{dt} \\ \frac{di'_b}{dt} \\ \frac{di'_c}{dt} \end{bmatrix} = \begin{bmatrix} \frac{-r}{L} & 0 & 0 \\ 0 & \frac{-r}{L} & 0 \\ 0 & 0 & \frac{-r}{L} \end{bmatrix} \begin{bmatrix} i'_g \\ i'_g \\ i'_c \\ i'_c \end{bmatrix} + \frac{1}{L} \begin{bmatrix} v'_q - (e_{a1} - e_{a2}) \\ v_b - (e_{b1} - e_{b2}) \\ v'_c - (e_{c1} - e_{c2}) \end{bmatrix}$$

Above equation represents the mathematical model of the cascaded two-level inverter-based multilevel STATCOM in the stationary reference frame. This model is transformed to the synchronously rotating reference frame [10]. The dq– axes reference voltage components of the converter and are controlled as

$$e_{d}^{*} = -x_{1} + \omega Li_{q}^{'} + v_{d}^{'}$$
$$e_{q}^{*} = -x_{2} - \omega Li_{d}^{'} + v_{q}^{'}$$





Fig. 2. Cascaded two-level inverter-based multilevel STATCOM



Fig. 3. Equivalent circuit of the cascaded two level inverter-based multilevel STATCOM

The control block diagram is shown in Fig. 4. The unit signals and are generated from the phase-locked loop (PLL) using three-phase supply voltages [13]. The converter currents are transformed to the synchronous rotating reference frame using the unit signals. The switching frequency ripple in the converter current



e-ISSN: 2348-6848, p- ISSN: 2348-795X Volume 3, Issue 01, January 2016 Available at http://internationaljournalofresearch.org

components is eliminated using a low-pass filter (LPF). From and loops, the controller generates – axes reference voltages, and for the cascaded inverter. With these reference voltages, the inverter supplies the desired reactive current

and draws required active current to regulate total dclink voltage. However, this will not ensure that individual dc-link voltages are controlled at their respective reference values. Hence, additional control is required to regulate individual dc-link voltages of the inverters.



Fig. 4. Control block diagram of proposed system

Network voltages are unbalanced due to asymmetric faults or unbalanced loads [13]. As a result, negative-sequence voltage appears in the supply voltage. This causes a double supply frequency component in the dc-link voltage of the inverter. This double frequency component injects the third harmonic component in the ac side [13]. Moreover, due to negative-sequence voltage, large negative-sequence current flows through the inverter which may cause the STATCOM to trip. Therefore, during unbalance, the inverter voltages are controlled in such a way that either negative-sequence current flowing into the inverter is eliminated or reduces the unbalance in the grid voltage. In the latter case, STATCOM needs to supply large currents since the interfacing impedance is small. This may lead to tripping of the converter.

All the mathematical calculated simulation parameters are given in the Appendix section.

III. MATLAB BASED SIMULATION & IT'S RESULTS

Fig.5. & Fig.6. Shows the MATLAB based simulation diagram of proposed system. The system configuration shown in Fig. 1 is considered for simulation. The simulation study is carried out using MATLAB/ SIMULINK.



Fig.5. MATLAB/Simulink based proposed system diagram with masked blocks

Reactive power is directly injected into the grid by setting the reference reactive current component at a particular value. Initially, is set at 0.5 p.u. At 2.0 s, is changed to 0.5 p.u. Fig. 7(a) shows the source voltage and converter current of the phase. Fig. 7(b) shows the dc-link voltages of two inverters. From the figure, it can be seen that the dc-link voltages of the inverters are regulated at their respective reference values when the STATCOM mode is changed from capacitive to inductive





e-ISSN: 2348-6848, p- ISSN: 2348-795X Volume 3, Issue 01, January 2016 Available at http://internationaljournalofresearch.org



Fig.6. MATLAB based simulation diagram of operation during fault. (a) Grid voltages on the LV side of the transformer. (b) d-axis negative-sequence current component. (c) q-axis negative-sequence current component

Fig. 9. MATLAB based simulation diagram of operation during fault. (a) Grid voltages on the LV side of the transformer. (b) d-axis negative-sequence current component. (c) q-axis negative-sequence current component with fuzzy logic controller



Fig. 9. MATLAB based simulation diagram of operation during fault. (a) Grid voltages on the LV side of the transformer. (b) d-axis negative-sequence current component. (c) q-axis negative-sequence current component with fuzzy logic controller

APPENDIX TABLE .I.SIMULATION SPECIFICATIONS

Parameter	Rating
Transformer voltage ratings	11kV/400 kV
AC frequency supply	50 Hz
Transformer resistance	3%

Dc Link capacitors	50µF
Rated Power	5MVA
Transformer leakage	15%
reactance	
Inverter-1 dc Link	659 V
voltage	
Inverter-2 dc Link	241 V
voltage	

IV. CONCLUSION

DC-link voltage balance is one of the major issues in cascaded inverter-based STATCOMs. In this paper, a simple var compensating scheme is proposed for a cascaded two-level inverter-based multilevel inverter. The scheme ensures regulation of dc-link voltages of inverters at asymmetrical levels and reactive power compensation. The performance of the scheme is validated by simulation and experimentations under balanced and unbalanced voltage conditions. Further, the cause for instability when there is a change in reference current is investigated. The dynamic model is developed and transfer functions are derived. System behavior is analyzed for various operating conditions. From the analysis, it is inferred that the system is a non minimum phase type, that is, poles of the transfer function always lie on the left half of the -plane. However, zeros shift to the right half of the -plane for certain operating conditions. For such a system, oscillatory instability for high controller gains exists.

REFERENCES

[1] B. Singh, R. Saha, A. Chandra, and K. Al Haddad, "Static synchronous compensators (STATCOM): A review," *IET Power Electron.*, vol. 2, no. 4, pp. 297–324, 2009.

[2] H. Akagi, H. Fujita, S. Yonetani, and Y. Kondo, "A 6.6-kV transformerless STATCOM based on a fivelevel diode-clamped PWM converter: System design and experimentation of a 200-V 10-kVA laboratory model," *IEEE Trans. Ind. Appl.*, vol. 44, no. 2, pp. 672–680, Mar./Apr. 2008.

[3] H. Akagi, S. Inoue, and T. Yoshii, "Control and performance of a transformerless cascaded PWM STATCOM with star configuration," *IEEE Trans. Ind. Appl.*, vol. 43, no. 4, pp. 1041–1049, Jul./Aug. 2007.



e-ISSN: 2348-6848, p- ISSN: 2348-795X Volume 3, Issue 01, January 2016 Available at http://internationaljournalofresearch.org

[4] H. P. Mohammadi and M. T. Bina, "A transformerless medium-voltage STATCOM topology based on extended modular multilevel converters," *IEEE Trans. Power Electron.*, vol. 26, no. 5, pp. 1534–1545, May 2011.

[5] N. N. V. Surendra Babu, D. Apparao, and B. G. Fernandes, "Asymmetrical dc link voltage balance of a cascaded two level inverter based STATCOM," in *Proc., IEEE TENCON*, 2010, pp. 483–488.

[6] A. Leon, J. M. Mauricio, J. A. Solsona, and A. Gomez-Exposito, "Software sensor-based STATCOM control under unbalanced conditions," *IEEE Trans. Power Del.*, vol. 24, no. 3, pp. 1623–1632, Jul. 2009.

[7] Y. Suh, Y. Go, and D. Rho, "A comparative study on control algorithm for active front-end rectifier of large motor drives under unbalanced input," *IEEE Trans. Ind. Appl.*, vol. 47, no. 3, pp. 825–835, May/Jun. 2011.

[8] S. Laali, K. Abbaszades, and H. Lesani, "New hybrid control methods based on multi-carrier PWM techniques and charge balance control methods for cascaded multilevel converters," in *Proc. CCECE*, 2011 pp. 243–246.

[9] J. Napoles, A. J. Watson, and J. J. Padilla, "Selective harmonic mitigation technique for cascaded Hbridge converter with nonequal dc link voltages," *IEEE Trans. Ind. Electron.*, vol. 60, no. 5, pp. 1963–1971, May 2013.

[10] N. Farokhnia, S. H. Fathi, N. Yousefpoor, and M. K. Bakhshizadeh, "Minimisation of total harmonic distortion in a cascaded multilevel inverter by regulating of voltages dc sources," *IET Power Electron.*, vol. 5, no. 1, pp. 106–114, Jan. 2012.

[11] Welflen Ricardo Nogueira Santos , Edison Roberto Cabral da Silva and Cursino Brandao Jacobina , "The Transformerless Single-Phase Universal Active Power Filter for Harmonic and Reactive Power Compensation", IEEE Transactions on Power Vol.29 , No.7 , pp. 3563- 3572 July 2014

[12] Y. Tang, P. C. Loh, P. Wang, F. H. Choo, F. Gao, and F. Blaabjerg, "Generalized design of high performance shunt active power filter with output lcl filter," *IEEE Trans. Ind. Electron.*, vol. 59, no. 3, pp. 1443–1452, Mar. 2012

[13] E. Babaei, "Optimal topologies for cascaded submultilevel converters," *J. Power Electron.*, vol. 10, no. 3, pp. 251–261, May 2010.

[14] E. Babaei, S. Alilu, and S. Laali, "A new general topology for cascaded multilevel inverters with reduced number of components based on developed H-bridge,"

IEEE Trans. Ind. Electron., vol. 61, no. 8, pp. 3932–3939, Aug. 2014.

[15] J. Ebrahimi, E. Babaei, and G. B. Gharehpetian, "A new topology of cascaded multilevel converters with reduced number of components for high-voltage applications," *IEEE Trans. Power Electron.*, vol. 26, no. 11,

pp. 3119-3130, Nov. 2011.

[16] A. Luo, S. Peng, C. Wu, J. Wu, and Z. Shuai, "Power electronic hybrid system for load balancing compensation and frequency-selective harmonic suppression," *IEEE Trans. Ind. Electron.*, vol. 59, no. 2, pp. 723–732, Feb. 2012.

[17] Q.-N. Trinh and H.-H. Lee, "An advanced current control strategy for three-phase shunt active power filters," *IEEE Trans. Ind. Electron.*, vol. 60, no. 12, pp. 5400–5410, Dec. 2013.

[18] S. Laali, K. Abbaszades, and H. Lesani, "A new algorithm to determine the magnitudes of dc voltage sources in asymmetrical cascaded multilevel converters capable of using charge balance control methods," in *Proc. ICEMS*, Incheon, Korea, 2010, pp. 56–61.

[19] M. F. Kangarlu and E. Babaei, "A generalized cascaded multilevel inverter using series connection of sub-multilevel inverters," *IEEE Trans. Power Electron.*, vol. 28, no. 2, pp. 625–636, Feb. 2013.

[20] J. Pereda and J. Dixon, "Cascaded multilevel converters: Optimal asymmetries and floating capacitor control," *IEEE Trans. Ind. Electron.*, vol. 60, no. 11, pp. 4784–4793, Nov. 2013.

[21] E. Babaei, M. Farhadi Kangarlu, and F. Najaty Mazgar, "Symmetric and asymmetric multilevel inverter topologies with reduced switching devices," *Elect. Power Syst. Res.*, vol. 86, pp. 122–130, May 2012.