



# Fuzzy Logic Controlled based PFC Cuk Converter Fed BLDC Motor Drive

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**Abstract**—a bridgeless single phase ac-dc rectifier based Cuk derived converter topology fed BLDC motor is proposed to improve power factor at the AC mains near to the unity with low THD for PFC applications. It utilizes one control signal over the whole line cycle. The most effective method of power quality improvement is also simulated using MATLAB/Simulink. It utilizes one control signal over the whole line cycle. In addition, the proposed converter exhibits low inrush current and low magnetic emissions as classical Cuk topology. The partial elimination of diodes in DBR in the bridgeless topology results in lower conduction losses as compared with conventional Cuk converter. The proposed method is simulated in MATLAB/Simulink with PI and fuzzy logic controller for precise speed control. A diode bridge rectifier (DBR) followed by a Cuk converter working in discontinuous conduction mode (DCM) is used for control DC link voltage with unity power factor at AC mains. The fuzzy based controller system is used for general purpose industrial applications.

**Index Terms**— CCM, Cuk converter, DCM, PFC, BLDC Motor, Power Quality, Fuzzy Logic Control.

## INTRODUCTION

Efficiency and cost are the major concerns in the development of low-power motor drives targeting household applications such as fans, water pumps, blowers, mixers, etc. The use of the brushless direct current (BLDC) motor in these applications is becoming very common due to features of high efficiency, high flux density per unit volume, low maintenance requirements, and low electromagnetic interference problems [1]. These BLDC motors are not limited to household applications, but these are suitable for other applications such as medical equipment, transportation, HVAC, motion control, and many industrial tools [2]–[4]. A BLDC motor has three phase windings on the stator and permanent magnets on the rotor [5], [6]. The BLDC motor is also known as an electronically commutated motor because an electronic commutation based on rotor position is used rather than a mechanical commutation which has disadvantages like sparking and wear and tear of

brushes and commutator assembly [7]. Power quality problems have become important issues to

be considered due to the recommended limits of harmonics in supply current by various international power quality standards such as the International Electro technical Commission (IEC) 61000-3-2 [8]. For class-a equipment (< 600 W, 16 A per phase) which includes household equipment, IEC 61000-3-2 restricts the harmonic current of different order such that the total harmonic distortion (THD) of the supply current should be below 19% [9].

Low power motor drives such as fans, water pumps, blowers, mixers, HVAC transmission, motion control etc. use BLDC motor for their efficient operation. Since BLDC offers high efficiency, low electromagnetic interference, low maintenance and high flux density per unit volume, we use BLDC for low power applications. BLDC motors are very popular in a wide variety of applications. Compared with a DC motor, the BLDC motor uses an electric commutator rather than a mechanical commutator, so it is more reliable than the DC motor. In a BLDC motor, rotor magnets generate the rotor's magnetic flux, so BLDC motors achieve higher efficiency. Therefore, BLDC motors may be used in high-end white goods (refrigerators, washing machines, dishwashers, etc.), high-end pumps, and fans and in other appliances which require high reliability and efficiency. In this respect, the BLDC motor is equivalent to a reversed DC commutator motor, in which the magnet rotates while the conductors remain stationary. In the DC commutator motor, the current polarity is altered by the commutator and brushes [10-13].

In recent years, the number and variety of applications of Fuzzy Logic (FL) have increased significantly. To understand why use of Fuzzy Logic has grown, it must be first understood as what is

meant by Fuzzy Logic. Fuzzy Logic has two different meanings. In a narrow sense, Fuzzy Logic is a logical system, which is an extension of multivalve logic. However, in a wider sense Fuzzy Logic is almost synonymous with the theory of Fuzzy sets, a theory which relates to classes of objects with unsharp boundaries in which membership is a matter of degree. In this perspective, Fuzzy logic in its narrow sense is a branch of Fuzzy Logic. Even in its more narrow definition, Fuzzy logic differs both in concept and substance from traditional multivalve logical systems.

## II. SYSTEM CONFIGURATION

Figs.1-2 show the PFC Cuk converter based VSI fed BLDC motor drive using a current multiplier and a voltage follower approach respectively. A high frequency metal oxide semiconductor field effect transistor (MOSFET) is used in Cuk converter for PFC and voltage control, whereas insulated gate bipolar transistor's (IGBT) are used in the VSI for its low frequency operation. BLDC motor is commutated electronically to operate the IGBT's of VSI in fundamental frequency switching mode to reduce its switching losses. The PFC Cuk converter operating in CCM using a current multiplier approach is shown in Fig. 1 i.e. the current flowing in the input and output inductors ( $L_i$  and  $L_o$ ), and the voltage across the intermediate capacitor ( $C_1$ ) remains continuous in a switching period. Whereas, Fig.2 shows a Cuk converter fed BLDC motor drive operating in DCM using a voltage follower approach. The current flowing in either of the input or output inductor ( $L_i$  and  $L_o$ ) or the voltage across the intermediate capacitor ( $C_1$ ) become discontinuous in a switching period for a PFC Cuk converter operating in DCM. A Cuk converter is designed to operate in all three discontinuous conduction modes and a continuous conduction mode of operation and its performance is evaluated for a wide voltage control with unity power factor at AC mains.

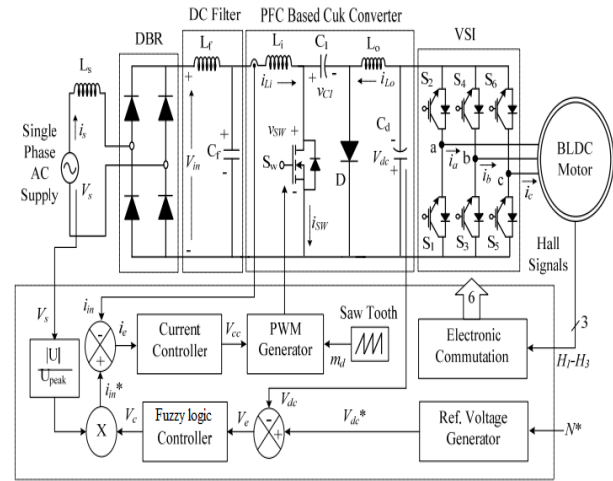


Fig.1. A BLDC Motor Drive Fed by a PFC Cuk Converter Using A Current Multiplier Approach With Fuzzy Logic Controller.

## III. OPERATION OF CUK CONVERTER IN DIFFERENT MODES

The operation of Cuk converter is studied in four different modes of CCM and DCM. In CCM, the current in inductors ( $L_i$  and  $L_o$ ) and voltage across intermediate capacitor  $C_1$  remain continuous in a switching period. Moreover, the DCM operation is further classified into two broad categories of discontinuous inductor current mode (DICM) and discontinuous capacitor voltage mode (DCVM). In DICM, the current flowing in inductor  $L_i$  or  $L_o$  becomes discontinuous in their respective modes of operation. While in DCVM operation, the voltage appearing across the intermediate capacitor  $C_1$  becomes discontinuous in a switching period. Different modes for operation of CCM and DCM are discussed as follows.

### A. CCM Operation

The operation of Cuk converter in CCM is described as follows. Figs.3 (a) and (b) show the operation of Cuk

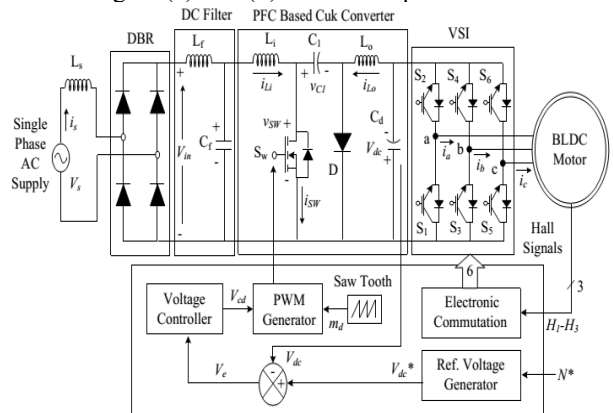


Fig.2. A BLDC Motor Drive Fed by a PFC Cuk Converter Using a Voltage Follower Approach.

Converter in two different intervals of a switching period and Fig.3(c) shows the associated waveforms in a complete switching period. Interval I: When switch  $S_{wm}$

turned on, inductor  $L_i$  stores energy while capacitor  $C_1$  discharges and transfers its energy to DC link capacitor  $C_d$  as shown in Fig.3(a). Input inductor current  $i_{L_i}$  increases while the voltage across the intermediate capacitor  $V_{C_1}$  decreases as shown in Fig.3(c). Interval II: When switch  $S_w$  is turned off, then the energy stored in inductor  $L_o$  is transferred to DC link capacitor  $C_d$ , and inductor  $L_i$  transfers its stored energy to the intermediate capacitor  $C_1$  as shown in Fig.3 (b). The designed values of  $L_i$ ,  $L_o$  and  $C_1$  are large enough such that a finite amount of energy is always stored in these components in a switching period.

### B. DICM ( $L_i$ ) Operation

The operation of Cuk converter in DICM ( $L_i$ ) is described as follows. Figs.4(a)-(c) show the operation of Cuk converter in three different intervals of a switching period and Fig.4(d) shows the associated waveforms in a switching period. Interval I: When switch  $S_w$  is turned on, inductor  $L_i$  stores energy while capacitor  $C_1$  discharges through switch  $S_w$  to transfer its energy to the DC link capacitor  $C_d$  as shown in Fig.4 (a). Input inductor current  $i_{L_i}$  increases while the voltage across the capacitor  $C_1$  decreases as shown in Fig.4 (d). Interval II: When switch  $S_w$  is turned off, then the energy stored in inductor  $L_i$  is transferred to intermediate capacitor  $C_1$  via diode  $D$ , till it is completely discharged to enter DCM operation. Interval III: During this interval, no energy is left in input inductor  $L_i$ , hence current  $i_{L_i}$  becomes zero. Moreover, inductor  $L_o$  cooperates in continuous conduction to transfer its energy to DC link capacitor  $C_d$ .

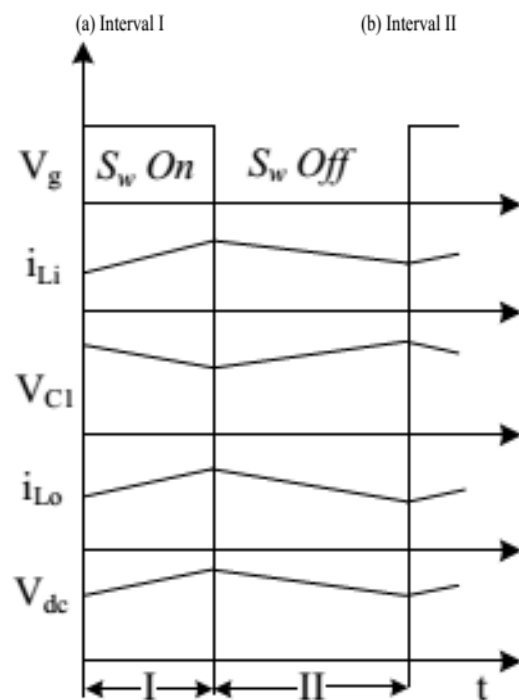
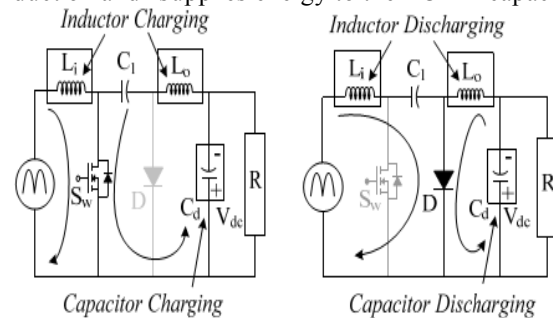
### C. DICM ( $L_o$ ) Operation

The operation of Cuk converter in DICM ( $L_o$ ) is described as follows. Figs.5(a)-(c) show the operation of Cuk converter in three different intervals of a switching period and Fig.5(d) shows the associated waveforms in a switching period. Interval I: As shown in Fig.5(a), when switch  $S_w$  is turned on, inductor  $L_o$  stores energy while capacitor  $C_1$  discharges through switch  $S_w$  to transfer its energy to the DC link capacitor  $C_d$ . Interval II: When switch  $S_w$  is turned off, then the energy stored in inductor  $L_i$  and  $L_o$  is transferred to intermediate capacitor  $C_1$  and DC link capacitor  $C_d$  respectively. Interval III: In this mode of operation, the output inductor  $L_o$  is completely discharged hence its current  $i_{L_o}$  becomes zero. An inductor  $L_i$  operates in continuous conduction to transfer its energy to the intermediate capacitor  $C_1$  via diode  $D$ .

### D. DCVM ( $C_1$ ) Operation

The operation of Cuk converter in DCVM ( $C_1$ ) is described as follows. Figs.6(a)-(c) show the operation of Cuk converter in three different intervals of a switching period and Fig. 6(d) shows the associated waveforms in a switching period. Interval I: When switch  $S_w$  is turned

on as shown in Fig.6 inductor  $L_o$  stores energy while capacitor  $C_1$  discharges through switch  $S_w$  to transfer its energy to the DC link capacitor  $C_d$  as shown in Fig.6 (d). Interval II: The switch is in conduction state but intermediate capacitor  $C_1$  is completely discharged, hence the voltage across it becomes zero. Output inductor  $L_o$  continues to supply energy to the DC link capacitor. Interval III: As the switch  $S_w$  is turned off, input inductor  $L_i$  starts charging the intermediate capacitor, while the output inductor  $L_o$  continues to operate in continuous conduction and supplies energy to the DC link capacitor.



(c) Waveforms

Fig.3. Operation Of Cuk Converter In CCM During (A-B) Different Intervals Of Switching Period And (C) The Associated Waveforms.

## IV. DESIGN OF A PFC CUK CONVERTER

A PFC based Cuk converter fed BLDC motor drive is designed for DC link voltage control of VSI with power factor correction at the AC mains. The Cuk converter is

designed for a CCM and three different DCMs. In DCM, any one of the energy storing elements  $L_i$ ,  $L_o$  or  $C_d$  are allowed to operate in discontinuous mode whereas in CCM, all these three parameters operate in continuous conduction. The design and selection criterion of these three parameters is discussed in the following section. The input voltage  $V_s$  applied to the DBR is given as,

$$V_s(t) = V_m \sin(2\pi f_L t) = 220\sqrt{2} \sin(314t) \quad (1)$$

Where  $V_m$  is the peak input voltage (i.e.  $\sqrt{2}V_s$ ,  $V_s$  is the rms value of supply voltage),  $f_L$  is the line frequency i.e. 50 Hz. The instantaneous voltage appearing after the DBR is as,

$$V_{in}(t) = |v_m \sin(t)| = |220\sqrt{2} \sin(314t)| \quad (2)$$

Where  $|\cdot|$  represents the modulus function. The output voltage,  $V_{dc}$  of Cuk converter is given as

$$V_{dc} = \frac{D}{(1-D)} V_{in}(t) \quad (3)$$

Where  $D$  represents the duty ratio. The instantaneous value of duty ratio,  $D(t)$  depends on the Input voltage appearing after DBR,  $V_{in}(t)$  and the required DC link voltage,  $V_{dc}$ .

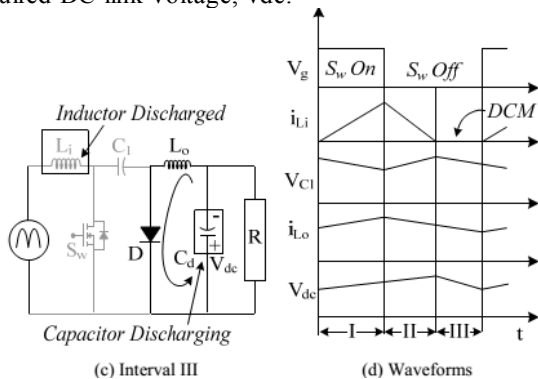


Fig. 4. Operation of Cuk converter in DICM ( $L_i$ ) during (a-c) different intervals of switching period and (d) the associated waveforms.

Hence the instantaneous duty ratio,  $D(t)$  is obtained by substituting (2) in (3) and rearranging it as,

$$D(t) = \frac{V_{dc}}{V_{in}(t) + V_{dc}} = \frac{V_{dc}}{|V_m \sin(\omega t)| + V_{dc}} \quad (4)$$

The Cuk converter is designed to operate from a minimum DC voltage of 40V ( $V_{dc \min}$ ) to a maximum DC link voltage of 200V ( $V_{dc \max}$ ). The PFC converter of maximum power rating of 350W ( $P_{\max}$ ) is designed

for a BLDC motor of 251W ( $P_m$ ) (full specifications given in Table I) and the switching frequency ( $f_s$ ) is taken as 20kHz. Since the speed of the BLDC motor is controlled by varying the DC link voltage of the VSI, hence the instantaneous power,  $P_{iatt}$  any DC link voltage ( $V_{dc}$ ) can be taken as linear function of  $V_{dc}$ . Hence for a minimum value of DC link voltage as 40V, the minimum power is calculated as 70W.

#### A. Design of $L_i$

For Continuous or Discontinuous Current Conduction the critical value of input inductor  $L_{ic}$  is expressed as

$$L_{ic} = \frac{V_{in}(t)D(t)}{2I_{in}(t)f_s} = \frac{R_{in}D(t)}{2f_s} = \left(\frac{V_s^2}{P_i}\right) \frac{D(t)}{2f_s} = \frac{1}{2f_s} \left(\frac{V_s^2}{P_i}\right) \frac{V_{dc}}{V_{in}(t) + V_{dc}} \quad (5)$$

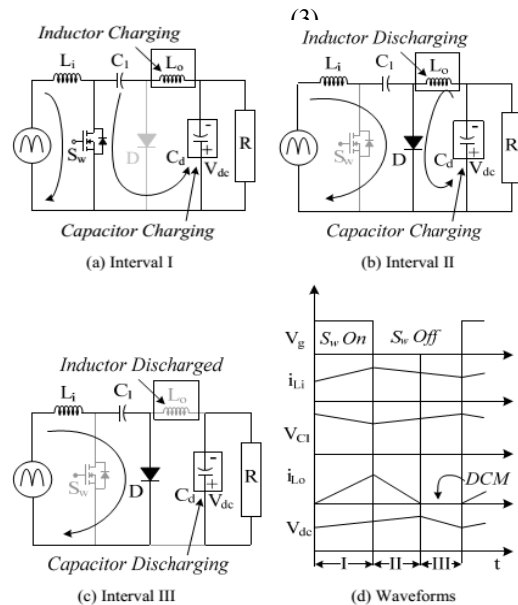


Fig.5. Operation of Cuk converter in DICM ( $L_o$ ) during (a-c) different intervals of switching period and (d) the associated waveforms.

Hence the critical value of input side inductor is directly proportional to the rms value of supply voltage; therefore the worst case design occurs for the minimum value of supply voltage (i.e.  $V_s = V_{s \min} = 85V$ ). Now the critical value of input inductor at the maximum DC link voltages of 200V at the peak value of supply voltage (i.e.  $\sqrt{2}V_{s \min}$ ) is calculated as,

$$I_{ic200} = \frac{1}{2fs} \left( \frac{Vs_{min}^2}{P_{max}} \right) \cdot \frac{V_{dcmax}}{\sqrt{2Vs_{min} + V_{dcmax}}} \\ = \frac{1}{2 \times 20000} \left( \frac{85^2}{350} \right) \left( \frac{200}{85\sqrt{2} + 200} \right) = 322.3 \mu H \quad (6)$$

And the critical value of input inductor at the minimum value of DC link voltages of 40V at the peak value of supply voltage is calculated as

$$I_{ic40} = \frac{1}{2fs} \frac{Vs_{min}^2}{P_{min}} \cdot \left( \frac{V_{dcmin}}{\sqrt{2Vs_{min} + V_{dcmin}}} \right) \\ = \frac{1}{2 \times 20000} \left( \frac{85^2}{70} \right) \left( \frac{40}{85\sqrt{2} + 40} \right) = 644.25 \mu H \quad (7)$$

Hence the value of critical input inductance is obtained lower at maximum DC link voltage. Therefore, the critical value of input inductor is selected lower than Lic200. The Performance of the Cuk converter feeding BLDC motor drive is analyzed for different values of input side inductor i.e.

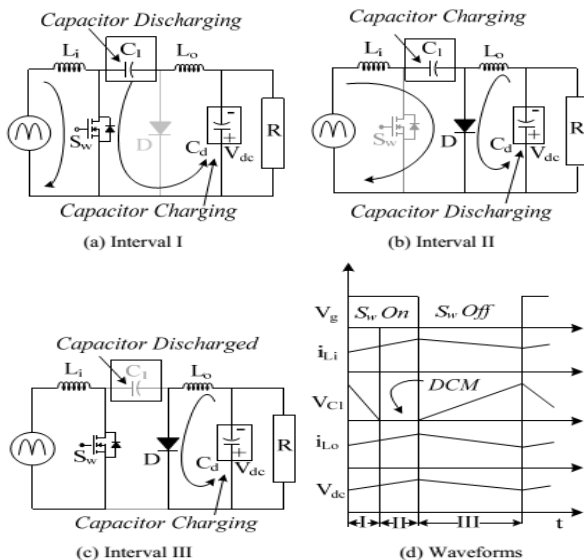


Fig.6. Operation of Cuk converter in DCM (C1) during (a-c) different intervals of switching period and (d) the associated waveforms.

A high THD of AC mains current is obtained at higher values of input side inductor which doesn't comply with the IEC 61000-3-2 [14]. Hence the input inductor (Li) of the order of 100μH is selected for its operation in discontinuous conduction to achieve a low value of THD of supply current at AC mains. The value of input inductor to operate in CCM is decided by the amount of permitted ripple current (η) and is as,

$$L_{iccm} = \frac{V_{in}(t)D(t)}{\eta I_{in}(t)fs} = \frac{R_{in}D(t)}{\eta fs} = \left( \frac{Vs^2}{Pi} \right) \frac{D(t)}{\eta fs} \\ = \frac{1}{\eta fs} \left( \frac{Vs^2}{Pi} \right) \frac{V_{dc}}{V_{in}(t) + V_{dc}} \quad (8)$$

The maximum inductor ripple current is obtained at the rated condition i.e. Vdc=200V for a minimum supply voltage (Vs min =85V). Hence the input side inductor is designed at the peak value of minimum supply voltage (i.e. Vs=√2Vsmin) as,

$$L_{oc} = \frac{V_{dc}(1-D(t))}{2I_{lo}(t)fs} = \frac{V_{dc}D(t)}{2I_{in}(t)fs} = \frac{R_{in}V_{dc}D(t)}{2V_{in}(t)fs} \\ = \left( \frac{Vs^2}{Pi} \right) \frac{V_{dc}}{2V_{in}(t)fs} \left( \frac{V_{dc}}{V_{in}(t) + V_{dc}} \right) \quad (9)$$

Where the permitted amount of ripple current is selected as 25% of the input current. Hence the input side inductor of 2.5mH is selected for its operation in continuous conduction.

#### V.FUZZY LOGIC CONTROL

L. A. Zadeh presented the first paper on fuzzy set theory in 1965. Since then, a new language was developed to describe the fuzzy properties of reality, which are very difficult and sometime even impossible to be described using conventional methods. Fuzzy set theory has been widely used in the control area with some application to power system [5]. A simple fuzzy logic control is built up by a group of rules based on the human knowledge of system behavior. Matlab/Simulink simulation model is built to study the dynamic behavior of converter. Furthermore, design of fuzzy logic controller can provide desirable both small signal and large signal dynamic performance at same time, which is not possible with linear control technique. Thus, fuzzy logic controller has been potential ability to improve the robustness of compensator.

The basic scheme of a fuzzy logic controller is shown in Fig 7 and consists of four principal components such as: a fuzzy fication interface, which converts input data into suitable linguistic values; a knowledge base, which consists of a data base with the necessary linguistic definitions and the control rule set; a decision-making logic which, simulating a human decision process, infer the fuzzy control action from the knowledge of the control rules and linguistic variable definitions; a de-fuzzification interface which yields non fuzzy control action from an inferred fuzzy control action [10].

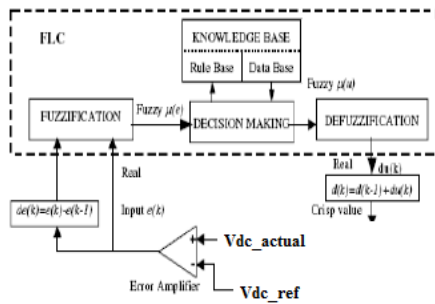


Fig.7 Block diagram of the Fuzzy Logic Controller (FLC) for Proposed Converter.

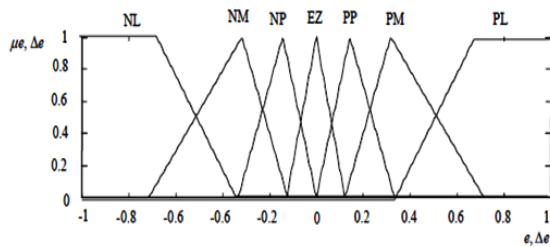


Fig.8 Membership functions for Input, Change in input, Output. Rule Base: the elements of this rule base table are determined based on the theory that in the transient state, large errors need coarse control, which requires coarse input/output variables; in the steady state, small errors need fine control, which requires fine input/output variables. Based on this the elements of the rule table are obtained as shown in Table 1, with 'Vdc' and 'Vdc-ref' as inputs.

$e \backslash \Delta e$	NL	NM	NS	EZ	PS	PM	PL
NL	NL	NL	NL	NL	NM	NS	EZ
NM	NL	NL	NL	NM	NS	EZ	PS
NS	NL	NL	NM	NS	EZ	PS	PM
EZ	NL	NM	NS	EZ	PS	PM	PL
PS	NM	NS	EZ	PS	PM	PL	PL
PM	NS	EZ	PS	PM	PL	PL	PL
PL	NL	NM	NS	EZ	PS	PM	PL

**VLMATLAB/SIMULINK RESULTS**

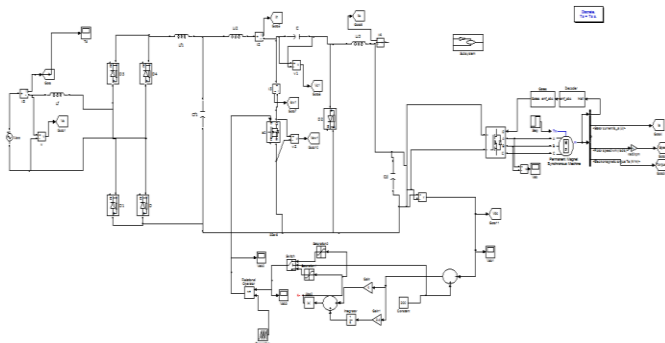


Fig.9. Matlab/Simulink Model of A BLDC Motor Drive Fed by a PFC Cuk Converter with PI Controller.

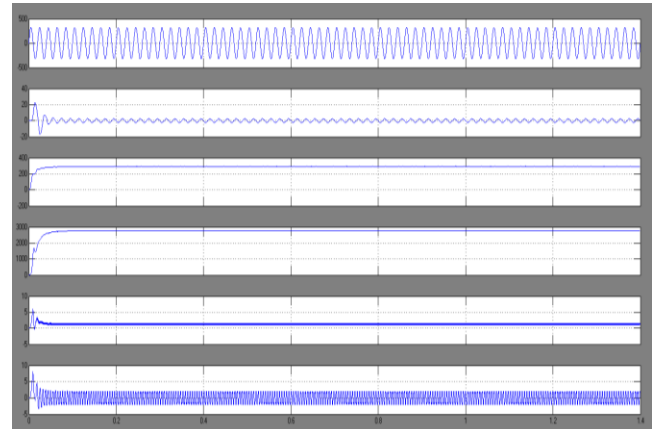


Fig.10. Simulated waveform Source Voltage and Current DC Voltage, Speed, Torque, Armature Current of BLDC motor drive with Cuk converter operating in CCM.

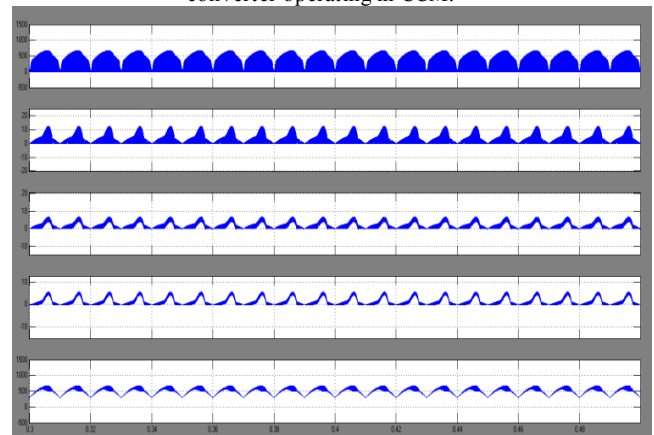


Fig.11. Simulation Waveform of Switch Voltage and Current, Inductor Current, Load Current and Capacitor Voltage of BLDC Motor Drive with Cuk Converter Operating in CCM.

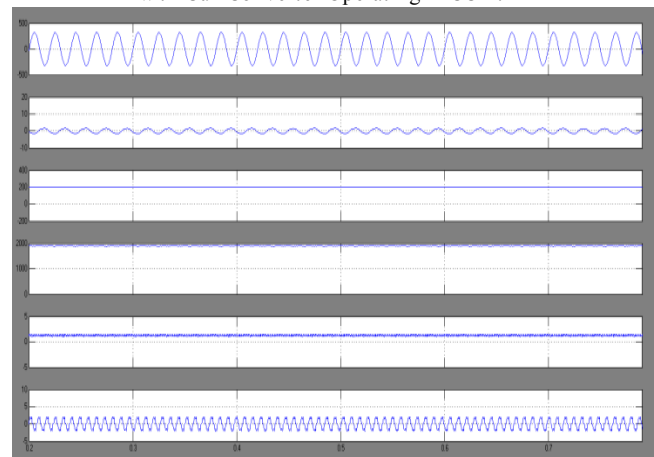


Fig.12. Simulated waveform Source Voltage and Current DC Voltage, Speed, Torque, Armature Current of BLDC motor drive with Cuk Converter Operating in DICM (Li).

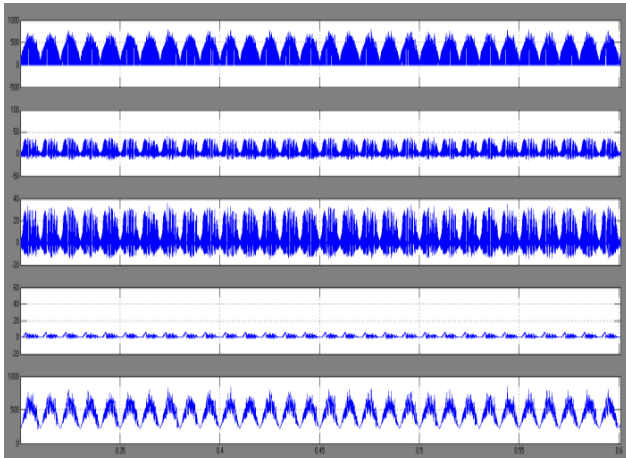


Fig.13.Simulation Waveform of Switch Voltage and Current, Inductor Current, Load Current and Capacitor Voltage of BLDC motor drive with Cuk Converter Operating in DICM (Li).

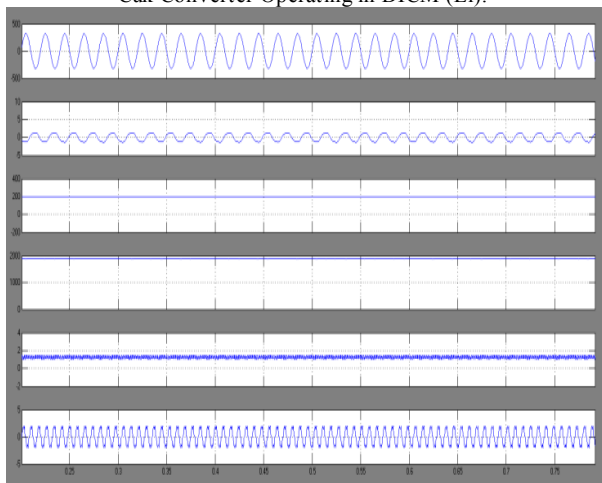


Fig.14.Simulated waveform Source Voltage and Current DC Voltage, Speed, Torque, Armature Current of BLDC motor drive with Cuk Converter Operating in DICM (Lo).

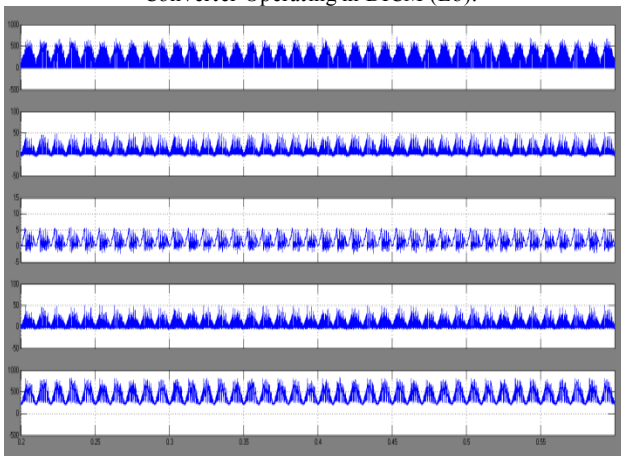


Fig.15. Simulation Waveform of Switch Voltage and Current, Inductor Current, Load Current and Capacitor Voltage of BLDC motor drive with Cuk converter operating in DICM (Lo).

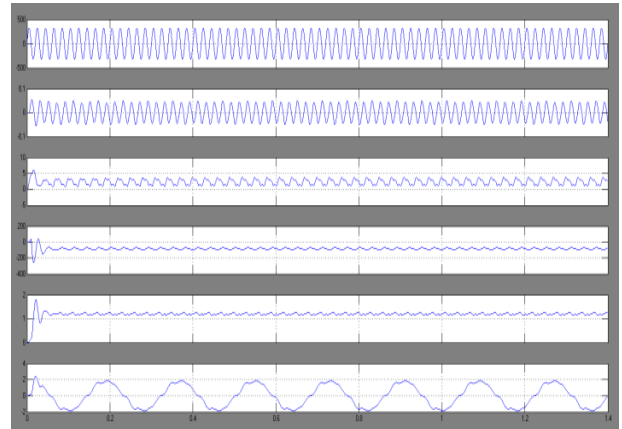


Fig.16.Simulated waveform Source Voltage and Current DC Voltage, Speed, Torque, Armature Current of BLDC motor drive with Cuk converter operating in DCVM.

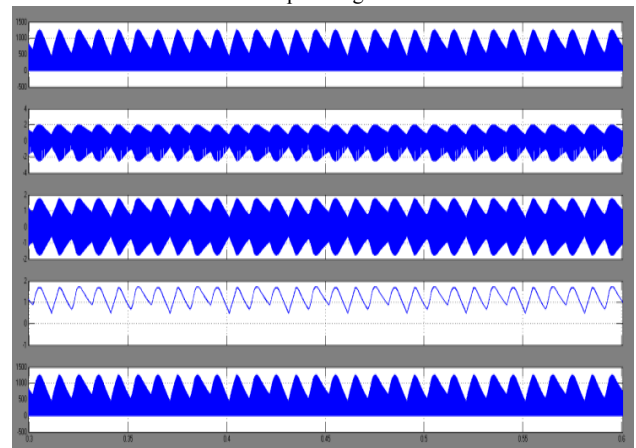


Fig.17. Simulation Waveform of Switch Voltage and Current, Inductor Current, Load Current and Capacitor Voltage of BLDC motor drive with Cuk converter operating in DCVM.

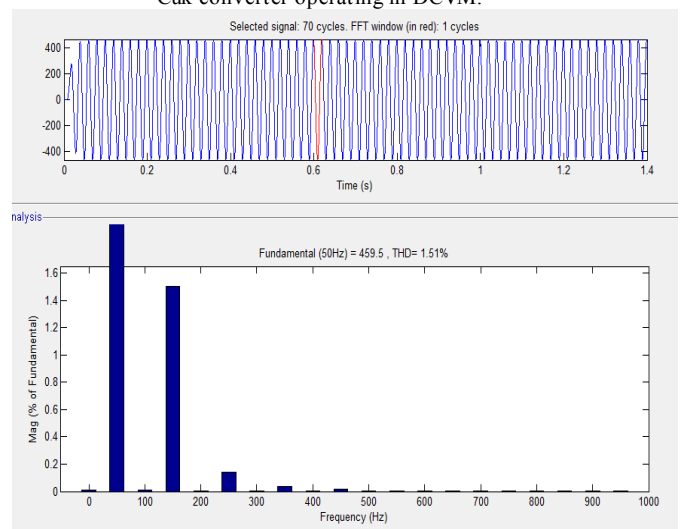


Fig.18.THD for Source Current with PI Controller.

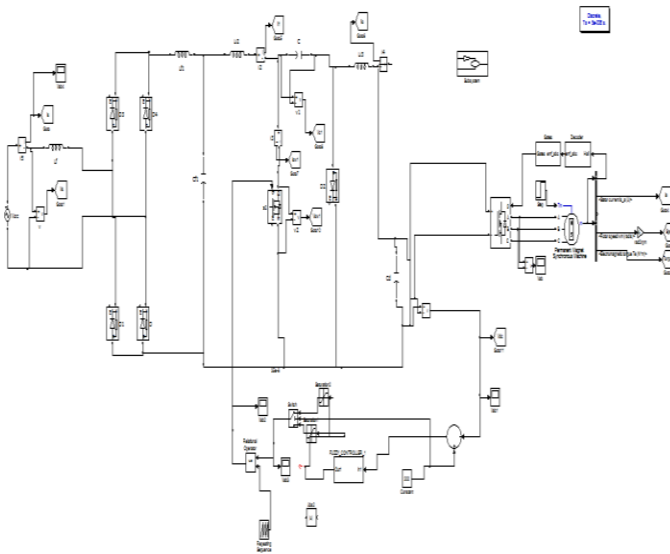


Fig.19. Matlab/Simulink model of A BLDC Motor Drive Fed by a PFC Cuk Converter with Fuzzy Logic Controller.

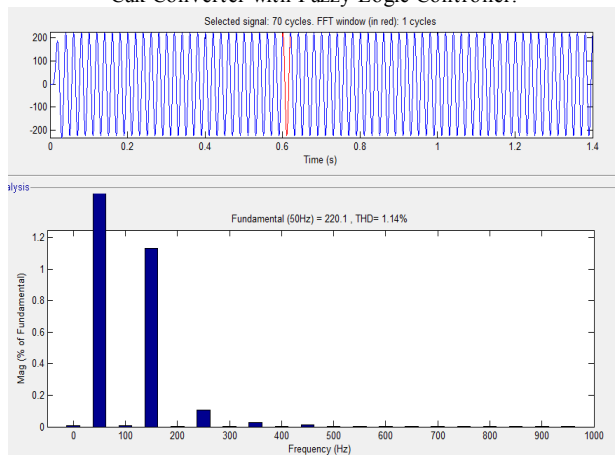


Fig.20. THD for Source Current with Fuzzy Logic Controller.

## VILCONCLUSION

The speed of the BLDC motor drive has been controlled by varying the DC link voltage of VSI; which allows the VSI to operate in fundamental frequency switching mode for reduced switching losses. Four different modes of Cuk converter operating in CCM and DCM have been explored for the development of BLDC motor drive with unity power factor at AC mains. A detailed comparison of all modes of operation has been presented on the basis of feasibility in design and the cost constraint in the development of such drive for low power applications. The proposed drive system has shown satisfactory results in all aspects and is a recommended solution for low power BLDC motor drives. The suitable controller for PFC operation of BLDC motor drives has been analysed.

FLC seems to be the best controller in performance improvement of BLDC motor drives for attaining the power factor near to unity. Moreover, voltage and current stresses on the fuzzy based PFC switch have been evaluated for determining the practical application of the proposed scheme. The proposed drive has been developed to validate the performance of the proposed BLDC motor drive under speed control with improved power quality at ac mains. The proposed scheme has shown satisfactory performance, and it is a recommended solution applicable to low-power BLDC motor drives.

## REFERENCES

- [1] J. F. Gieras and M. Wing, Permanent Magnet Motor Technology - Design and Application, Marcel Dekker Inc., New York, 2002.
- [2] C. L. Xia, Permanent Magnet Brushless DC Motor Drives and Controls, Wiley Press, Beijing, 2012.
- [3] Y. Chen, Y. C. Chiu, C. Y. Jhang, Z. Tang and R. Liang, "A Driver for the Single-Phase Brushless DC Fan Motor with Hybrid Winding Structure," IEEE Trans. Ind. Electron., Early Access, 2012.
- [4] S. Nikam, V. Rallabandi and B. Fernandez, "A high torque density permanent magnet free motor for in-wheel electric vehicle application," IEEE Trans. Ind. Appl., Early Access, 2012.
- [5] X. Huang, A. Goodman, C. Gelada, Y. Fang and Q. Lu, "A Single Sided Matrix Converter Drive for a Brushless DC Motor in Aerospace Applications," IEEE Trans. Ind. Electron., vol.59, no.9, pp.3542-3552, Sept. 2012.
- [6] W. Cui, Y. Gong and M. H. Xu, "A Permanent Magnet Brushless DC Motor With Bifilar Winding for Automotive Engine Cooling Application," IEEE Trans. Magnetics, vol.48, no.11, pp.3348-3351, Nov. 2012.
- [7] C. C. Hwang, P. L. Li, C. T. Liu and C. Chen, C, "Design and analysis of a brushless DC motor for applications in robotics," IET Elect. Pow. Appl., vol.6, no.7, pp.385-389, August 2012.
- [8] T. K. A. Brekken, H. M. Hapke, C. Stiller and J. Prudell, "Machines and Drives Comparison for Low-Power Renewable Energy and Oscillating Applications," IEEE Trans. Energy Convers., vol.25, no.4, pp.1162-1170, Dec. 2010.
- [9] N. Milivojevic, M. Krishnamurthy, A. Emadi and I. Stamenkovic, "Theory and Implementation of a Simple Digital Control Strategy for Brushless DC Generators," IEEE Trans. Power Electron., vol.26, no.11, pp.3345-3356, Nov. 2011
- [10] T. Kenjo and S. Nagamori, Permanent Magnet Brushless DC Motors, Clarendon Press, Oxford, 1985.
- [11] J. R. Handershot and T. J. E. Miller, Design of Brushless Permanent Magnet Motors, Clarendon Press, Oxford, 2010.
- [12] T. J. Sokira and W. Jaffe, Brushless DC Motors: Electronic Commutation and Control, Tab Books, USA, 1989.
- [13] H. A. Toliyat and S. Campbell, DSP-based Electromechanical Motion Control, CRC Press, New York, 2004.
- [14] Limits for Harmonic Current Emissions (Equipment input current  $\leq 16$  A per phase), International Standard IEC 61000-3-2, 2000.
- [15] N. Mohan, T. M. Undeland and W. P. Robbins, Power Electronics: Converters, Applications and Design, John Wiley and Sons Inc, USA,







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