

# Single-Phase High-Power Fuel Cell Converter With Direct Double-Frequency Ripple Current Control

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**ABSTRACT:** This project proposes a direct double-frequency ripple current control in a single-phase high-power fuel cell converter that can accomplish low-frequency ripple-free input current without using large electrolytic capacitors. Such a ripple current may reduce fuel cell life span. It tends to decrease the fuel cell output capacity because the fuel cell controller trips under instantaneous over-current condition. In this proposed method the content of ripples in current is reduced without requirement of extra switching devices. A fuel cell power system that contains a dc-ac inverter tends to draw an ac ripple current at twice the output frequency. Such a ripple current may reduce input cell life span. An advanced active control method is proposed to incorporate a current control loop in the dc-dc converter for ripple reduction.

**KEYWORDS:** Current-fed three-phase dc-dc converter, direct double-frequency ripple current control, electrolytic capacitor free, fuel cell.

## I. INTRODUCTION

Fuel cells are recognized as a future source of generating energy due to their efficient and clean energy characteristics, they produce low-varying dc voltage in the range of 30 to 60V for static power application such as residential usage. For static fuel cells, the power conditioning system consists of a low-voltage fuel cell as the primary source, a dc/dc converter to accomplish isolated high voltage, and a dc/ac inverter to connect commercial ac voltage. A dc/ac inverter supplies power into a 220V ac utility, an isolated dc/dc converter has to convert low varying dc voltage to high constant dc voltage about 370V. Therefore, a dc/dc converter with a high voltage ratio is needed, and a transformer is

normally employed for boosting voltage as well as isolation. However, high leakage inductance in the transformer leads to voltage spikes and electromagnetic noise. In order to accomplish a high voltage ratio while limiting the overshoot in the turn-off voltage produced by the leakage inductance, a current-fed dc/dc converter with an active clamp has been hosted in the push-pull topology and full-bridge topology for all single-phase application. In addition, a soft-switching active clamp scheme has been suggested to minimize turn-off losses in the clamp switch. These converters have been displayed to perform pretty well, but the single-phase circuits face severe components stress and degraded efficiency for higher power levels.

Fuel cells usually feature relatively low voltage and high current at the output terminals and thus require isolated power electronic interface. Current-fed (CF) converters are used more often than their voltage-fed (VF) counterparts, since low current ripple operation has a favorable impact over fuel cell lifetime and energy yield. Hence, this paper focuses on CF interface converters for medium and high power systems. In some cases, a single-phase converter implementation is not feasible due to limitations of existing power semiconductors and thermal management. There are several conventional possibilities to overcome those limitations. First, several converters with independent transformers can be connected in parallel at the input and output sides [3]-[9]. Output side of the parallel converters can be also connected in series in order to achieve higher DC voltage gain [10], [11]. Such

design enables high power operation, modularity, interleaved operation with lower current and voltage ripples, (N+1) redundancy, etc. In some high and medium power applications, when single phase converter implementation is complicated, three-phase DC-DC converter can be considered as a suitable solution. A three-phase isolated DC-DC converters were first proposed to overcome limitations of a single-phase counterparts in [12]. This approach does not provide as many advantages as multiphase parallel converters, while it requires only a single isolation transformer and thus can provide lower cost and higher power density.

Recently, numerous three-phase CF interface converters were introduced for fuel cell applications. Fuel cells relate to demanding application field, since they typically feature the highest output power and current at the lowest input voltage. It means that CF converter should provide the highest Dc voltage gain at the highest input current. Therefore, majority of three-phase CF interface converters proposed recently feature soft-switching to achieve high efficiency. Most of them utilize the active clamping circuits at either the input side, or the output side.

To achieve a high step-up gain with high efficiency in non-isolated applications, a high step-up method based on isolated-type converters is hosted. By piling the secondary side of an isolated converter in addition to its primary side, a high step-up conversion ratio and distributed voltage stress can be achieved. Moreover, a careful selection of an isolated converter can deliver zero-voltage switching (ZVS), continuous input current and reduced reverse recovery on diodes. A conventional voltage double rectifier boost-integrated half-bridge converter, the proposed converter satisfies all these features, which make appropriate for high step-up applications.

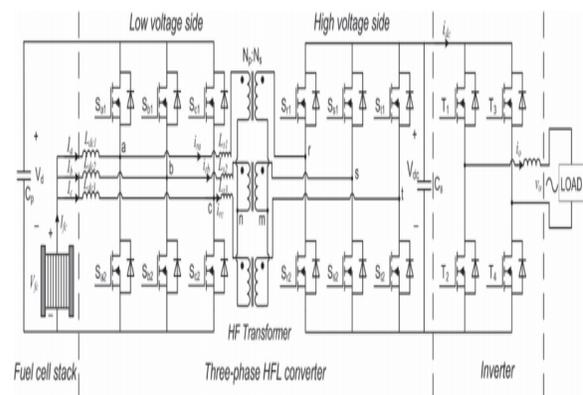
**DC-DC converter:** In many industrial applications, it is required to convert a fixed dc source into a variable voltage dc source. A dc-dc converter converts directly from dc-dc and simply known as a dc converter. A dc converter can be considered as dc equivalent to an ac transformer with an endlessly variable turn's ratio. Like a transformer, it can be

used to step down or step up a dc voltage source. Dc converters can be used as switching-mode regulators to convert a Dc voltage, normally unregulated to a regulated dc o/p voltage. This regulation is normally achieved by PWM at a fixed frequency and the switching device is normally BJT MOSFET IGBT. The designer can select the switching frequency by choosing the value of R, L, and C of frequency oscillator.

## II. SYSTEM MODELS

### A. Proposed Fuel Cell System Description

Fig. 1 shows the proposed two-stage HFL-based high-power fuel cell system. The system consists of a current-fed three-phase HFL converter with an isolated Y-Y connected high frequency (HF) transformer and an inverter. The three-phase HFL converter power flow is controlled by the phase shift angle  $\phi$  between the active switches on the low-voltage side (LVS) and the high-voltage side (HVS). The converter can be operated either in the boost mode or in the buck mode. The major features of this three-phase HFL converter have been studied. However, the method to reduce the input double-frequency ripple current caused by the inverter load has not been discussed.



(a)

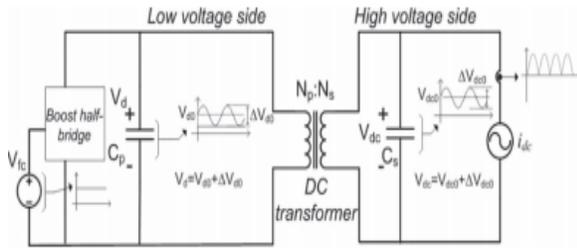


Fig. 1.(a) Proposed two-stage HFL-based high-power fuel cell power conditioning system.(b)Equivalent ripple circuit model of the proposed fuel cell system.

### B. Equivalent Ripple Circuit Modeling of the Proposed Fuel Cell System

Fig. 1(b) shows the equivalent ripple circuit model of the proposed fuel cell system.  $V_{fc}$  is the fuel cell stack voltage. If fuel cell current has negligible low-frequency ripple current,  $V_{fc}$  is the constant voltage. The dc-dc converter can be simplified as an ideal dc transformer since its switching frequency is much larger than the system ripple frequency. The inverter load is modeled as a double-frequency pulsation current source  $i_{dc}$ . As shown, both the LVS dc-bus voltage  $V_d$  and the HVS dc-bus voltage  $V_{dc}$  have the relatively large voltage swing. This control is designed based on the following three aspects.

- First, large voltage variation of  $V_{dc}$  leads to small HVS dc-bus capacitor  $C_s$ , which makes it viable to replace the electrolytic capacitor with a film capacitor. This has already been explained in [15].
- Second, if real-time balancing of transformer primary- and secondary-side voltages can be maintained by synchronizing  $V_d$  with primary-referred  $V_{dc}$ , the three-phase HFL converter can always maintain the ZVS operation. This will be further explained in the next section.
- Third, voltage variation on both LVS and HVS dc buses makes both the primary- and secondary-side capacitive energy sources ( $C_p$  and  $C_s$ , as shown in the circuit in Fig. 2) to

provide the ripple energy required by the inverter load.

### III. PROPOSED CONVERTER TOPOLOGY AND OPERATION ANALYSIS

This paper presents two-stage HFL-based high-power fuel cell system shows in Fig 2. The system consists of a current-fed 3-phase HFL converter with an isolated Y-Y connected high-frequency (HF) transformer and an inverter. The phase shift angle  $\phi$  controls the three-phase HFL converter power flow between the active switches on the low-voltage side (LVS) and the high-voltage side (HVS). The converter can be functioned either in the boost mode or in the buck mode. In this proposed method, the converter is operated in boost mode for fuel cell application. The boost function is achieved by the dc inductors ( $L_{dc1}$ ,  $L_{dc2}$ , and  $L_{dc3}$ ) and three half-bridges on the LVS. The leakage inductors ( $L_{s1}$ ,  $L_{s2}$ , and  $L_{s3}$ ) are the energy transfer element for each phase. This research focus is to study the direct double-frequency ripple current control of this three-phase HFL converter while connecting a single-phase inverter load.

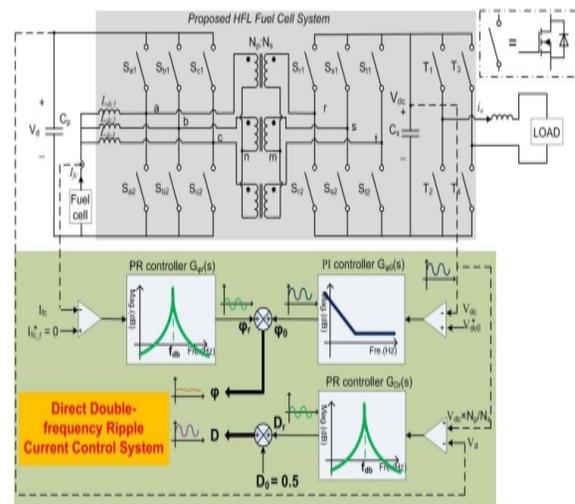


Fig.2 Proposed direct double-frequency ripple current control system diagram

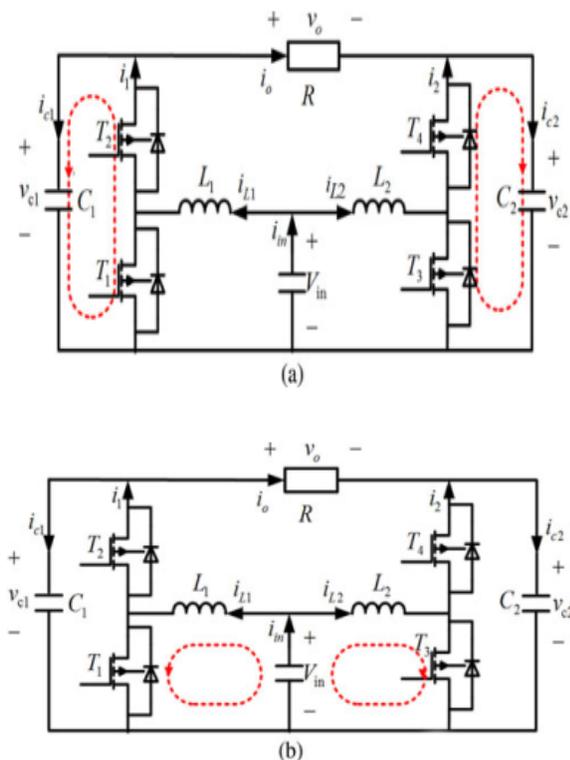


Fig. 3. Flow path of the double-line-frequency current component of the inverter. (a) With waveform control. (b) Without waveform control.

#### A. Effect of Capacitance Tolerance

Since the values of the capacitors  $C_1$  and  $C_2$  can affect the computation of the proposed waveform control, the effect of using a difference capacitance from that originally assumed in the computation on the control performance must be investigated. First, the parameters  $C_1$  and  $C_2$  are chosen as  $C_1 = C_2 = 15 \mu\text{F}$  for the voltage reference calculation adopted in waveform control. Then, a circuit simulation with  $C_1$  and  $C_2$  in the power stage varying from 5 to 25  $\mu\text{F}$  is performed. It is observed that a larger deviation of the capacitor value from the assumed value of 15  $\mu\text{F}$  leads to a poorer compensation of the double-line-frequency component. Yet, as the tolerance of the film capacitor is usually less than 10%, the effect of capacitance tolerance on the compensation capability is small (less than 8.19%), as given.

#### B. Further Remarks

The adoption of the proposed waveform control method to mitigate the low-frequency input current ripple will alter the original behavior of the differential inverter without waveform control. The following are important points to consider in terms of the adoption of waveform control:

- 1) there is no change in the desired ac output voltage even though the voltages of the capacitors themselves are altered;
- 2) the energy stored by the capacitors, which is a function of the voltages, is made up of a dc component and a double-line-frequency component;
- 3) DC energy is stored by the two capacitors while they supply ac energy to the output load. Consequently, the low-frequency power pulsation caused by ac output is absorbed by the capacitors while the fuel cells kept a constant supply of dc power to the capacitors;
- 4) as the capacitor voltages  $v_{c1}$  and  $v_{c2}$  are much higher than the dc input voltage  $v_{in}$ , the energy transfer will occur when the voltage fluctuation on  $C_1$  and  $C_2$  is increased.

An interesting point to take note is that since the capacitor voltages can be large without affecting the desired ac output voltage, both capacitors can be minimized without increasing the ripple voltage on the dc input. The advantage is that film capacitors can be used instead of electrolytic capacitors to improve reliability. The practical limit is the voltage rating of the capacitors.

#### IV. SIMULATION RESULTS

Using MATLAB/Simulink software, simulation was performed. MATLAB is a high performance language for technical computing and it integrates programming in an easy environment. Fig. 4 represents Simulink model of proposed high boost ratio transformer dc-dc converter. In this input voltage = 51V given to this converter. The voltage is stepped up using a three phase transformer and the

final DC voltage is obtained at the output side of the circuit.

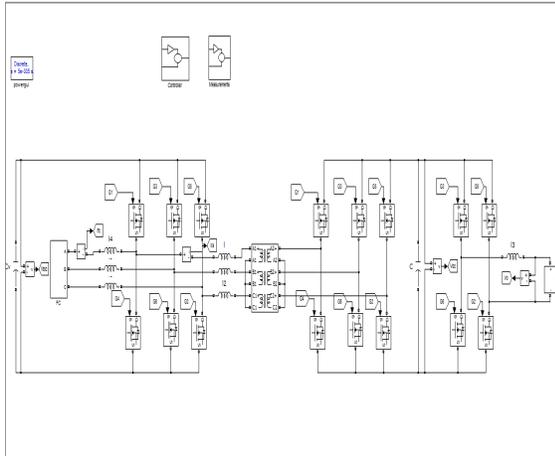


Fig .4Matlab/simulinkdiagram of two-stage HFL-based high-power fuel cell power conditioning system.

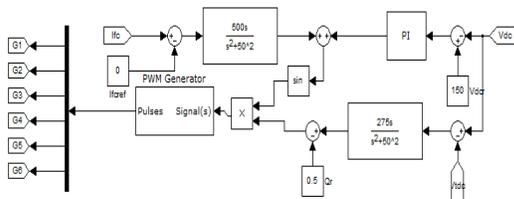


Fig .5 Controller subsystem

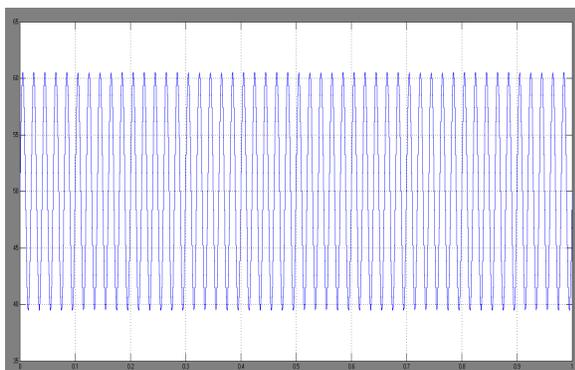


Fig .6Input VOLTAGE (VTDC)

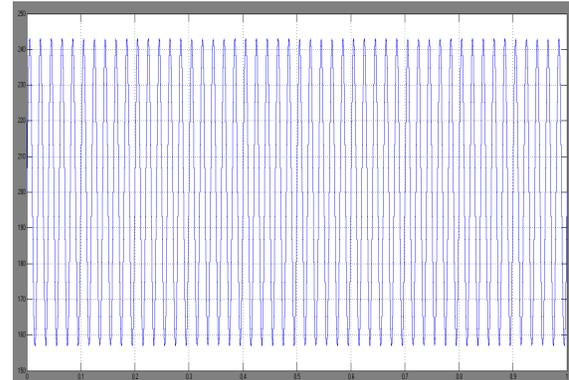


Fig .7 HVS dc-bus voltage (VDC)

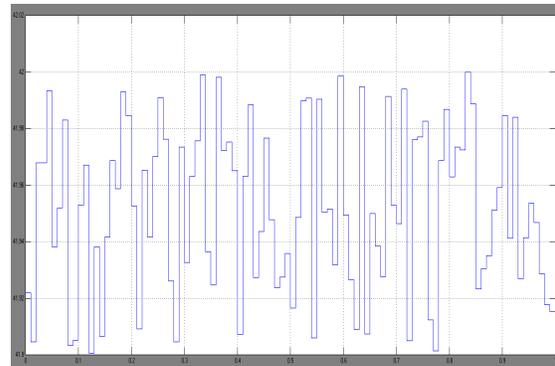


Fig .8Fuel cell current (IFC)

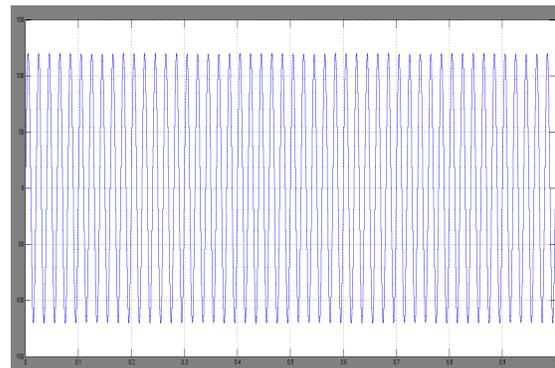


Fig.9 inverter output voltage (Vo)

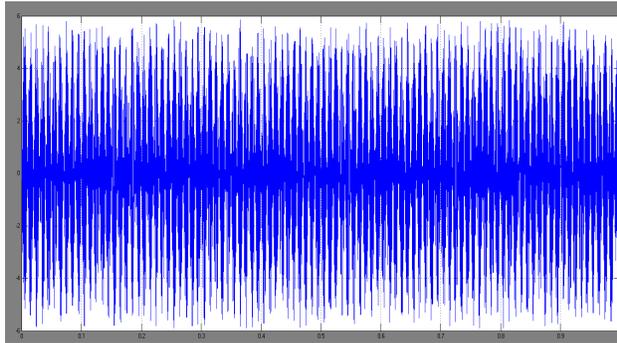


Fig. 10

## V. CONCLUSION

Three-phase HFL-based fuel cell power conditioning system that can accomplish low-frequency ripple-free input current by making use of direct double-frequency ripple current control. The proposed method can make full exploitation of capacitive ripple energy sources. The control system design based on the small-signal model has been analyzed in detail. To directly remove the fuel cell current double-frequency ripple, a PR controller is developed to achieve an extra high control gain at 120-Hz resonant frequency. This controller generates the virtual high impedance that can block the ripple energy propagation from inverter load to fuel cell stack, and it also eliminates the trouble from varied duty cycle.

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