

Asingle Phase Active Device for Power Quality Improvement of Electric Field Transportation

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Abstract: Problem statement: Now days, power quality has been given attention due to the intensive use of power electronic equipments in all types of industries such as steel, paper, textile industries and so on. These power electronic devices induce harmonic distortion into the supply lines which gives rise to many undesirable effects. **Approach:** This study presents a new method for harmonic and reactive power compensation with a Fuzzy logic controller and a new control algorithm for active power filter to eliminate harmonics and compensate the reactive power of three phase diode bridge rectifier with RL load. The Fuzzy logic controller was used to predict the reference current values and the firing pulses were generated using hysteresis current controller. The system was modeled and simulated using MATLAB/SIMULINK power system toolbox. **Results:** The total harmonic distortion for the system is reduced from 29.16-1.08% using the proposed fuzzy logic controller based shunt active filter. **Conclusion:** The simulation results found were quite satisfactory to eliminate harmonics and improve the power factor for non linearloads.

INTRODUCTION

Power quality is the ability of an electrical utility to provide electrical power without interruption and it encompasses any deviation from a perfect sinusoidal waveform. This includes transients, surges, sags, brownouts and harmonics. The growth in the use of non-linear loads has caused power quality problems like high current harmonics and low power factor (Chandra *et al.*, 2000; George and Basu, 2008; Asiminoaeiet *al.*, 2006). As it is becoming too important to prevent harmonic related problems, several harmonic standards have been developed and being followed by utilities worldwide. To avoid the effects of harmonics the passive filters and active filters are used. A passive filter has been a viable approach because of low cost and high efficiency. However, the passive scheme has limitations such as interference with the system impedance causing resonance with other networks and the inability to adapt to network characteristic variations (Wei *et al.*, 2006).

Active filters have advantages over passive filters by utilizing a switch mode power electronic converter to supply harmonic currents equal to those in the load

control, a Fuzzy Logic Controller (FLC) Model gives comparatively better harmonic reduction than the conventional PI Controllers (Singh and Solanki, 2009; Zaveriet *al.*, 2009; Ahmed *et al.*, 2009; Rathika and Devaraj, 2010). The advantages of fuzzy control are that it does not require accurate mathematical model, can work with imprecise inputs, can handle nonlinearity and are more robust than other conventional nonlinear controllers (Ghasemiet *al.*, 2008; Kerrouche and

currents (Singh and Singhal, 2007; Singh *et al.*, 2007; Chatchanayuenyong, 2009) and also minimize the reactive power. Active filters have the ability to adjust the amplitude of the synthesized ac voltage of the inverters by means of PWM by control of dc link voltage, thus drawing either leading or lagging power from the supply. The active filter attempts to restore the sinusoidal characteristics of the line current by injecting the opposite harmonics demanded by the load. In order to produce the harmonic cancellation effect, the APF is connected in parallel with the load. The objective is to force the source current to be sinusoidal and in phase with the source voltage to have zero Total Harmonic Distortion (THD) and unitary power factor at the source line.

Generally, the performance of APF is based on design of VSI, type of the firing circuit and methods used for calculating the reference current (Sharmeelaet *al.*, 2006). Several control algorithms and performance analysis were implemented using shunt active filter (Ajami and Hosseini, 2006; Kukrer and Komurcugil, 2008; Singh and Solanki, 2009; Zaveriet *al.*, 2009; Rahmaniet *al.*, 2010; Santiprapan and Areerak, 2010; Rani and Porkumaran, 2010). For power quality Karim, 2009; Reddy and Subramanyam, 2009; Moinuddin and Ram, 2010). The main objective of this study is to improve the power quality by developing a control algorithm for shunt active filter using fuzzy logic controller to eliminate the harmonics in power systems. A hysteresis controller based current controller was used and the simulation results are presented followed by the conclusion.

SYSTEM CONFIGURATION

current controller is employed in the inner loop control to perform the reference current calculation.

PROPOSED CONTROL ALGORITHM

The proposed control system of shunt active filter is concise and requires less computational efforts than many others found in the literature. It is formed by a DC voltage regulator and reference current estimator. Hysteresis controller is used for generating switching

The basic system configuration of the shunt active powerfilter is shown in Fig. 1. The Insulated-Gate Bipolar Transistor (IGBT) based Voltage Source Inverter (VSI) bridges with a common DC bus capacitor are used as the SAF. A hysteresis rule based carrier less Pulse Width Modulation (PWM) current control is employed to generate the gating signal to the switching devices. This system comprises three phase supply with diode bridge rectifier with RL as a non linear load (Chandra *et al.*, 2000) and the proposed shunt active filter is connected parallel to the system.

Only the load currents and source voltage are measured to force the line currents to be sinusoidal and in phase with the supply voltage. A proportional-integral voltage controller is used in the outer loop to maintain the dc bus voltage constant. The FLC based

signals for SAF to force the desired current into the system. The purposes of using the active filter are to (i) correct the power factor, (ii) regulate the DC voltage and (iii) eliminate the line harmonics. The flow chart of the control algorithm is given Fig.2.

The compensating currents of active filter are determined by sensing the load currents, DC bus voltage and peak voltage of AC source (V_{sm}). The instantaneous voltages of AC source can be represented as in Eq. 1:

$$\begin{aligned} V_{sa}(t) &= V_{sm} \times \sin(\omega t) \\ V_{sb}(t) &= V_{sm} \times \sin(\omega t - 120) \\ V_{sc}(t) &= V_{sm} \times \sin(\omega t - 240) \end{aligned} \quad (1)$$

The basic function of the proposed shunt active filter is to eliminate harmonics and compensate the current unbalance and reactive power of load. After compensating, the AC source feeds fundamental active power component of load current and losses of inverter for regulating the DC capacitor voltage and hence the peak of source reference current (I_{sm}) has two components. The first component represents the average load active power (I_{smp}^*) and the second component of AC source current (I_{smd}^*) is obtained from DC capacitor voltage regulator. Instantaneous power of load (at kth sample) is given by Eq.2:

$$P_{load}(k) = V_{sa}(k)I_{la}(k) + V_{sb}(k)I_{lb}(k) + V_{sc}(k)I_{lc}(k) \quad (2)$$

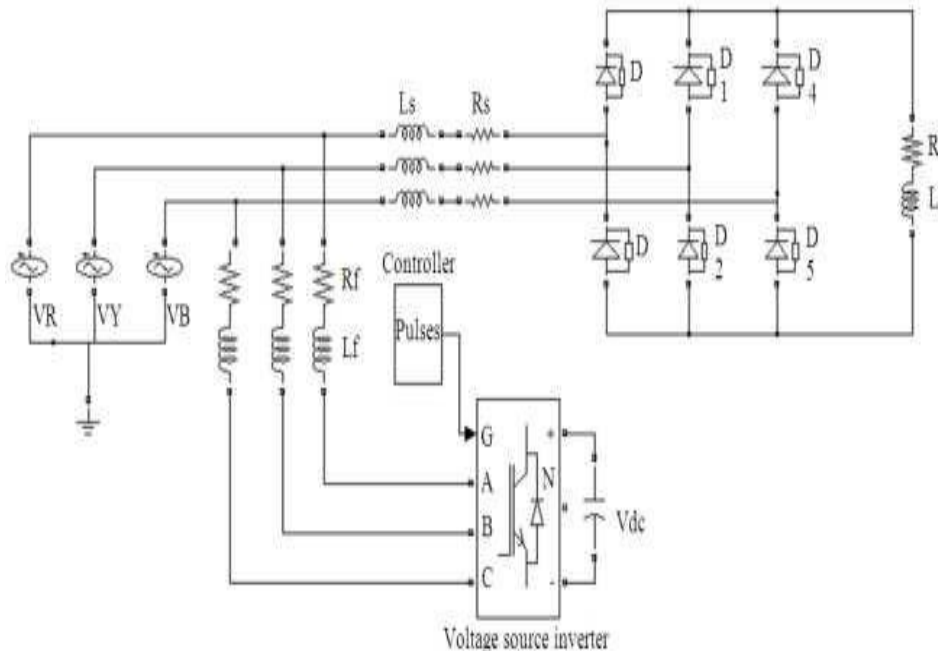


Fig. 1: Basic system with non-linear load and shunt active filter

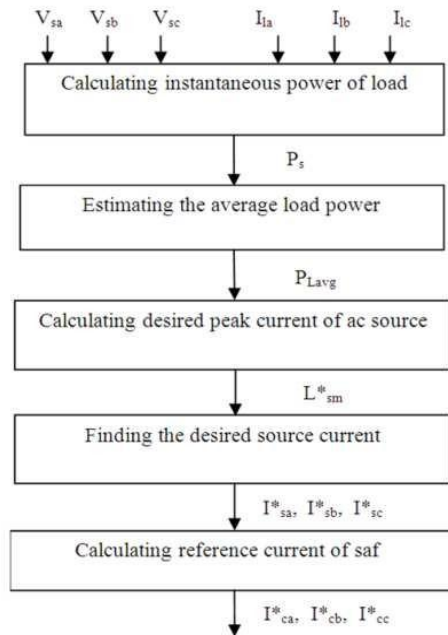


Fig. 2: The flow chart of the control algorithm

The average power of load (P_{Lavg}) is obtained by passing $P_{load}(k)$ to low-pass filter. The average power of load (P_{Lavg}) can be written by means of Eq. 3 and 4:

$$P_{lavg} = 1/n \sum_{k=1}^n P_{load}(k) \quad (3)$$

$$n = Tf_s; T = 1/f \quad (4)$$

Where:

f = The fundamental system frequency

f_s = The sampling frequency

In order to compensate the current harmonics and reactive power of load, the average active power of AC source must be equal to P_{Lavg} . Considering the unity power factor for AC source currents the average active power of AC source can be represented as Eq. 5:

$$P_s = 3/2 V_{sm} I_{smp}^* = P_{lavg} \quad (5)$$

From the average power of the load the first component of AC side current is obtained named I_{smp}^* and given as follows Eq. 6:

$$I_{smp}^* = 2/3 P_{Lavg} / V_{sm} \quad (6)$$

The second component of AC source current (I_{smd}^*) is obtained from DC capacitor voltage regulator as in Eq. 7,

where the difference between the reference value and the actual value is calculated and is given as:

$$V_{cdc}^* = V_{dcref} - V_{cdc} \quad (7)$$

This (V_{cdc}^*) will be given to the controller to obtain I_{smd}^* . The desired peak current of AC source is then obtained by the following expression Eq.8:

$$I_{sm}^* = I_{smp}^* + I_{smd}^* \quad (8)$$

The AC source current must be sinusoidal and in-phase with source voltages. Therefore the desired currents of AC source can be calculated by multiplying peak source current with unity sinusoidal signal and these unity signals are obtained by the following Eq.9:

$$\begin{aligned} U_a &= V_{sa} / V_{sm} \\ V_{sm} U_b &= V_{sb} / V_{sm} \\ V_{sm} U_c &= V_{sc} / V_{sm} \end{aligned} \quad (9)$$

The desired source current is given as Eq. 10:

$$\begin{aligned} I_{sa}^* &= I_{sm}^* \times U_a \\ I_{sb}^* &= I_{sm}^* \times U_b \\ I_{sc}^* &= I_{sm}^* \times U_c \end{aligned} \quad (10)$$

Finally, the reference currents of active filter can be obtained by subtracting the load current from the reference source current and given as follow Eq.11:

$$\begin{aligned} I_{ca}^* &= I_{sa}^* - I_{la} \\ I_{cb}^* &= I_{sb}^* - I_{lb} \\ I_{cc}^* &= I_{sc}^* - I_{lc} \end{aligned} \quad (11)$$

These reference currents will be given to the switching circuit of carrier-less hysteresis controller for producing the necessary PWM pulse to the voltage source inverter. So the voltage source inverter with the closed loop system acts as a controlled current source and produces the exact reference waveform at the output.

This output of the shunt active filter compensates the line harmonics and the line current becomes sinusoidal.

Role of DC side capacitor: When the APF is compensating the harmonic and reactive power components, the dc capacitor voltage V_{dc} varies. Hence V_{dc} is also sensed and regulated at a reference value V_{dc}^* in order to establish a self-sufficient energy at the dc bus. DC side capacitor serves two main purposes (i)

it maintains a dc voltage with small ripple in steady state and (ii) serves as an energy storage element to supply real power difference between load and source during transient period.

In steady state, the real power supplied by the source should be equal to the real power demand of the load plus a small power to compensate the losses in the active filter. Thus, the capacitor voltage can be maintained at a reference value. However, when the load condition changes the real power balance between the mains and the load will be disturbed. This real power difference is to be compensated by the dc capacitor. This changes the dc capacitor voltage away from the reference voltage.

In order to keep a satisfactory operation of the active filter, the peak value of the reference current must be adjusted to proportionally change the real power drawn from the source. This real power charged/discharged by the capacitor compensates the real power consumed by the load. If the dc capacitor voltage is recovered and the reference voltage is attained, the real power supplied by the source is supposed to be equal to that consumed by the load. Thus, in this fashion the peak value of the reference source current can be obtained by regulating the average voltage of the dc capacitor.

When the dc capacitor voltage is smaller than the reference voltage, it indicates that the real power supplied by the source is not enough to supply load demand and hence the source current (i.e. the real power drawn from the source) needs to be increased. On the other hand, a larger value of dc capacitor voltage tries to reduce the reference source current. DC capacitor design can be represented as Eq.12-14:

$$C = 2\Delta E / V_{ref}^2 - V_{min}^2 \quad (12)$$

Where:

$$V_{ref} = V_{max} + V_{min} / 2 \quad (13)$$

$$\Delta E = 1/2CV_{ref}^2 - 1.2 \quad (14)$$

FUZZY LOGIC CONTROL

Fuzzy Logic (FL) is a problem-solving control system methodology that lends itself to implementation in systems ranging from simple, small, embedded micro-controllers to large, networked, multi-channel PC or workstation-based data acquisition and control systems. It can be implemented in hardware, software, or a combination of both. FL provides a simple way to arrive at a definite conclusion based upon vague,

ambiguous, imprecise, noisy, or missing input information. FL approach to control problems mimics how a person would make decisions, but much faster. The concept of Fuzzy Logic (FL) is a way of processing data by allowing partial set membership rather than crisp set membership or non-membership. FL incorporates a simple, rule-based IF X AND Y THEN Z approach to solve a control problem rather than attempting to model a system mathematically.

The FLC mainly consists of three processes viz., Fuzzification, Inference and Defuzzification as shown in Fig.3.

Fuzzification: The fuzzy logic controller requires that each input/output variable which defines the control surface be expressed in fuzzy set notations using linguistic levels. The linguistic values of each input and output variable divide its universe of discourse into adjacent intervals to form the membership functions. The member value denotes the extent to which a variable belongs to a particular level. The process of converting input/output variable to linguistic levels is termed as fuzzification.

Inference: The behavior of the control surface which relates the input and output variables of the system are governed by a set of rules. A typical rule would be If X is A Then Y is B. When a set of input variables is read, each of the rules that have any degree of truth in its premise is fired and contributes to the forming of the control surface by approximately modifying it. When all the rules are fired, the resulting control surface is expressed as a fuzzy set to represent the constraint's output. This process is known as inference.

Defuzzification: Defuzzification is the process of converting a fuzzy quantity into a crisp quantity. There are several methods available for defuzzification, centroid method being the most prevalent one which uses the following formula for defuzzification Eq. 15:

$$\frac{\int (\mu(x)x) dx}{\int \mu(x) dx} \quad (15)$$

where, μ is the membership degree of outputx.

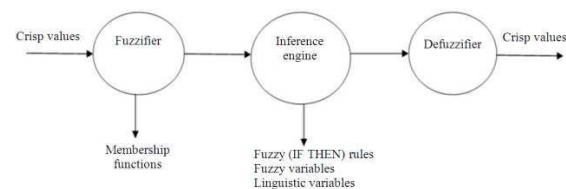


Fig. 3: Block diagram of FLC

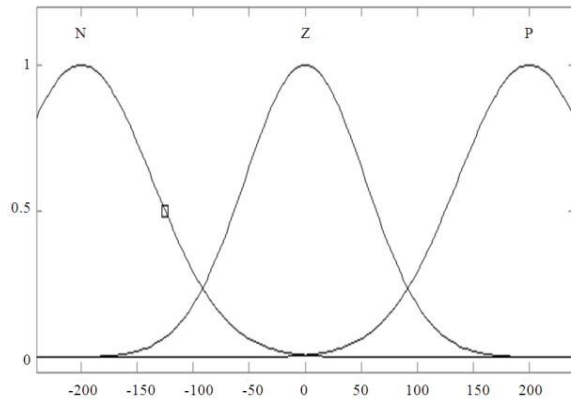


Fig. 4: Input membership function

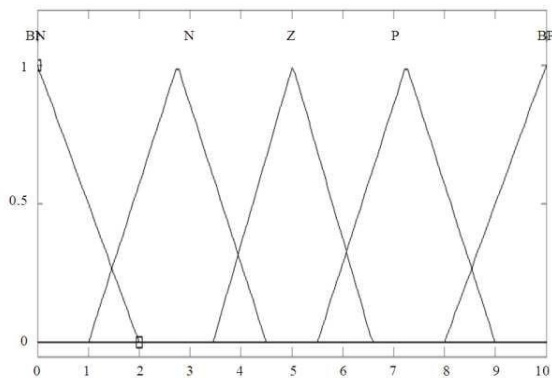


Fig. 5: Output membership function

Fuzzy logic implementation: To design a FLC, the variables which can represent the performance of the system to be controlled should be chosen as input to the controller. For the given system, the proposed control algorithm is formed by using three source voltages and three load currents as its input, the same six parameters are taken as input to the FLC. In the dc voltage controller side, the capacitor voltage deviation is considered as the input of the FLC. The real power requirement in terms of the reference current is taken as the output of the FLC. The input and output variables are in crisp form and they have to be converted into linguistic variable form.

Gauss membership function is chosen as the input varies in the sinusoidal form and it has three subsets (shown in Fig. 4). Since the crisp value from the sensor cannot be given as input to the fuzzy logic controller, the membership functions are used to convert the crisp value into linguistic value. The output values vary within a small range and hence triangular membership function is chosen (shown in Fig.5).

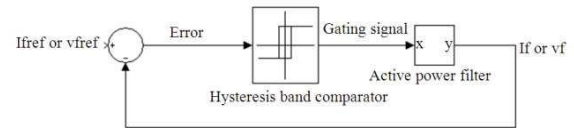


Fig. 6: Hysteresis current control

Table 1: Fuzzy rule representation

V	Negative	Zero	Positive
I	(N)	(Z)	(P)
Negative (N)	Big negative (BN)	Positive (P)	Big positive (BP)
Zero (Z)	Negative (N)	Zero (Z)	Positive (P)
Positive (P)	Big negative (BN)	Negative (N)	Big positive (BP)

Mamdani type fuzzy model was used for the implementation of the system. The input variables V1, V2 and V3 (ranging from -240-240V), I1, I2 and I3 (ranging from -10-10A) and the output variable I_{smd}^* (ranging from 0-10) were chosen. At the output defuzzification is done to obtain the crisp value. The relationship between the input and the output variable is chosen based on the Fuzzy rules representation table as shown in Table 1.

SWITCHING STRATEGY OF CONVERTER

Hysteresis current control is a method of generating the required triggering pulses by comparing the error signal with that of the hysteresis band and it is used for controlling the VSI so that the output current is generated from the filter will follow the reference current waveform is shown in Fig. 6. This method controls the switches in an inverter asynchronously to ramp the current through the inductor up and down to follow the reference. Though the hysteresis current control is the easiest method to implement, it has a disadvantage of having no limit to the switching frequency; however, an additional circuitry can be used to limit the maximum switching frequency. When the current through the inductor exceeds the upper hysteresis limit, a negative voltage is applied by the inverter to the inductor, which causes the current in the inductor to decrease. Once the current reaches the lower hysteresis limit, a positive voltage is applied to increase the current and the cycle repeats. The switching frequency can be altered by changing the width of the hysteresis band, the size of the inductor and the DC voltage applied to the inductor by the inverter. Hysteresis current control leads to asynchronous switching which produces a band of switching frequencies.

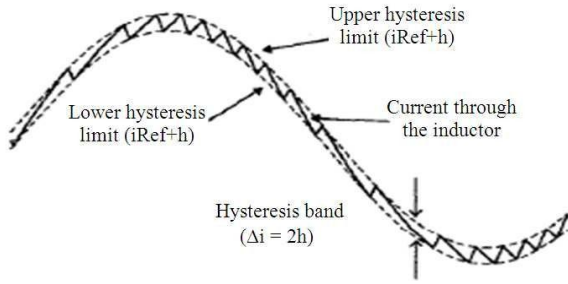


Fig. 7: Hysteresis band

Hysteresis band is shown in Fig. 7. If upper switch is OFF and lower switch is ON in first-leg.

If upper switch is ON and lower switch is OFF in the second-leg.

Similarly the switching logic of other two phases (b and c) of the SAF is formulated, using the width of hysteresis band.

MATERIALS AND METHODS

Simulation was carried out to demonstrate the effectiveness of the proposed control strategy for the active filter to reduce the harmonics. The test system used to carry out the analysis (Fig. 1) consists of a three phase voltage source and a three phase diode bridge rectifier with RL load. The active filter is connected to the test system through an inductor L. The values of the circuit elements used in the simulation are given in Table 2. MATLAB/SIMULINK is used to simulate the test system and the proposed shunt active filter.

RESULTS

The three phase source voltage and current which is same as that of the load waveform without shunt active filter is shown in Fig.8.

The frequency spectrum of the distorted waveform is shown in Fig. 9 where Total Harmonic Distortion (THD) of the distorted line current is 20.75%. From the harmonic spectrum, it is evident that, the supply current is distorted due to the harmonics especially of fifth and seventh order.

An active filter with fixed hysteresis band current control (HB = 0.5A) and a PI voltage control is connected in parallel with the load. Figure 10 shows the source voltage and source current of the system with the PI based conventional controller. The THD in this case has decreased from 20.75-1.27%.

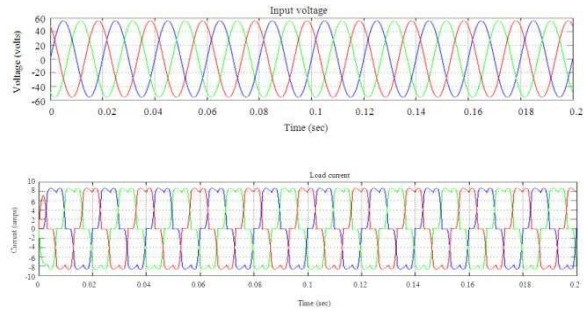


Fig. 8: Source voltage and current without filter

Table 2: System parameters

Parameters	Value
Supply peak voltage	56V
Supply frequency	50 Hz
V_{dc}	300mF
L_f	3mH
R_f	0.1Ω
K_p, K_i	0.001, 0.1
R_s	0.25Ω
L_s	2.5mH
R_l	10 Ω and 5Ω
L_l	5mH
Average switching frequency f_s	20kHz

Table 3: Comparison of results THD(%)

Method	R phase	Y phase	B phase
Without filter	29.16	29.13	29.14
Without FLC based filter	1.27	1.30	1.29
With FLC based filter	1.08	1.12	1.06

To reduce the harmonics further, the active filter was simulated with fuzzy logic based controller. Figure 11 shows the compensating current to be generated by using the proposed algorithm and the actual filter current that is injected in to the system is shown in Fig.

12. After the filter current is injected into the line, the source voltage and current waveforms are as shown in Fig. 13 and the frequency spectrum of the compensated current is shown in Fig.14.

The performance of the active filter with the proposed control algorithm is found to be satisfactory and the source current is eventually sinusoidal and it is in-phase with the supply voltage as shown in Fig.

13. The THD has decreased from 20.75-1.08% with fuzzy logic controller. Figure 15 shows the DC capacitor voltage for the shunt active power filter and it is clear that the controller is able to regulate the voltage requirement of the active filter. The Table 3 shows the percentage THD of supply current for PI based controller and FLC controller.

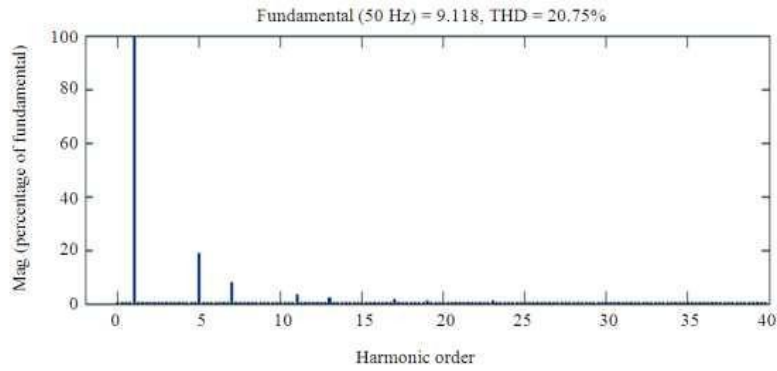


Fig. 9: Frequency spectrum of source current (R-phase) without filter

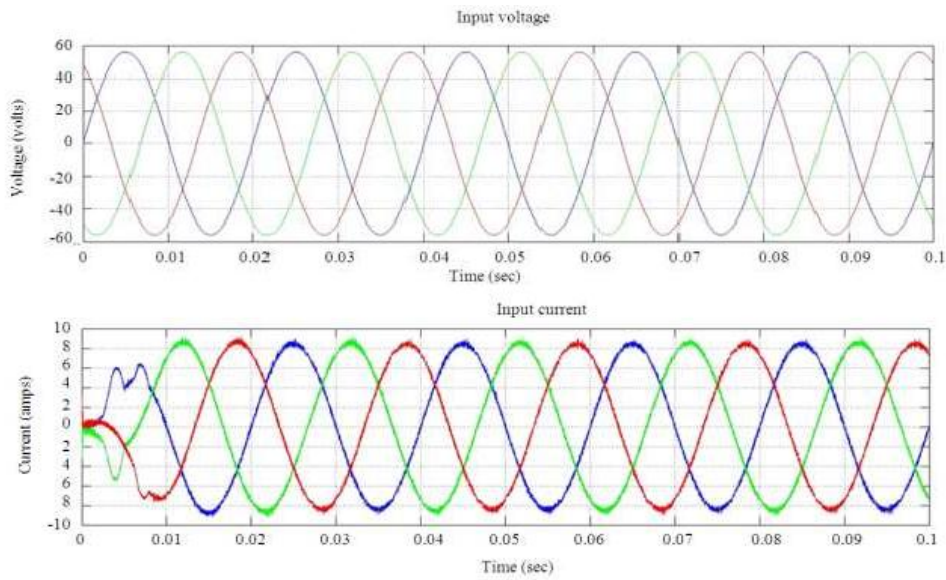


Fig. 10: Source voltage and current with PI based filter

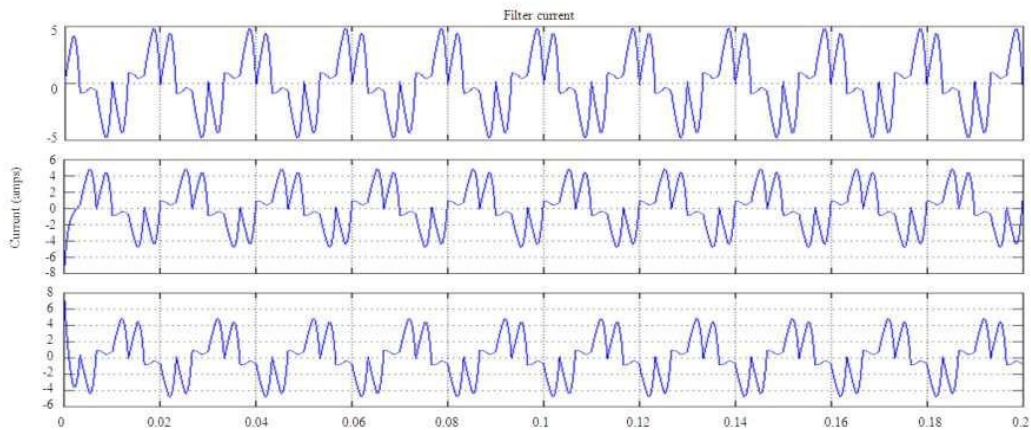


Fig. 11: Compensating current (a, b, c)

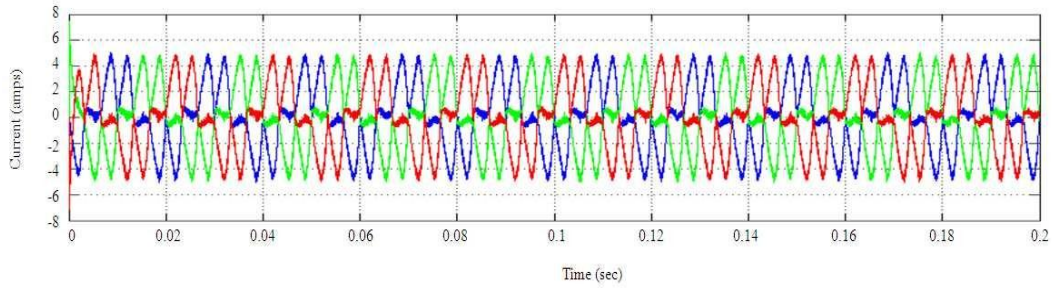


Fig. 12: Filter current (a, b, c)

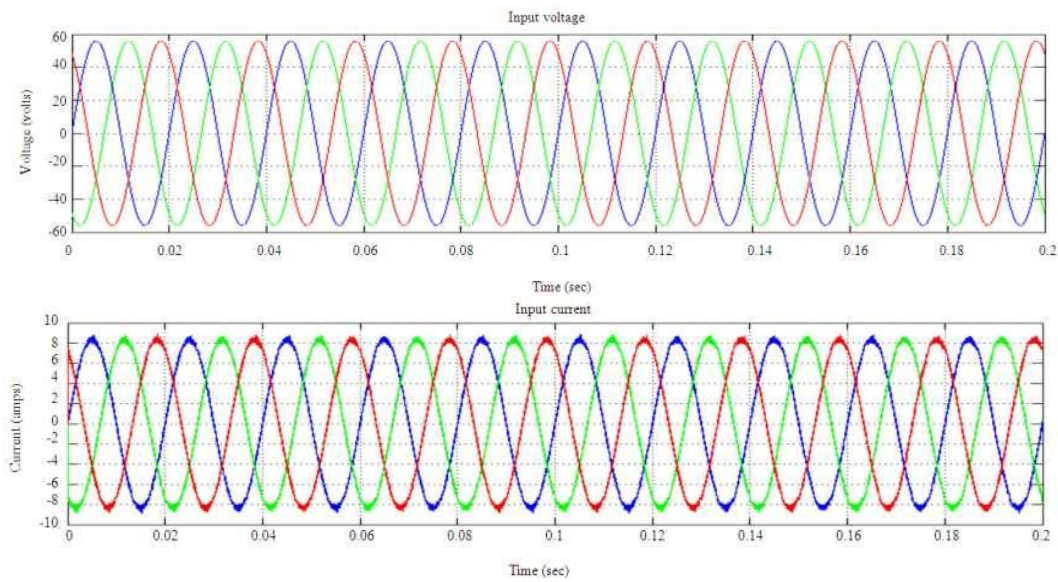


Fig. 13: Source voltage and source current with filter (a, b, c)

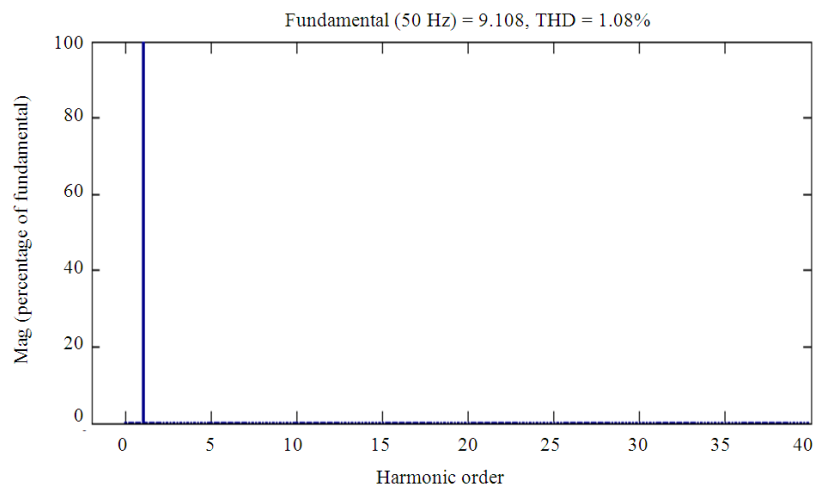


Fig. 14: Frequency spectrum of source current (R-phase) with SAF

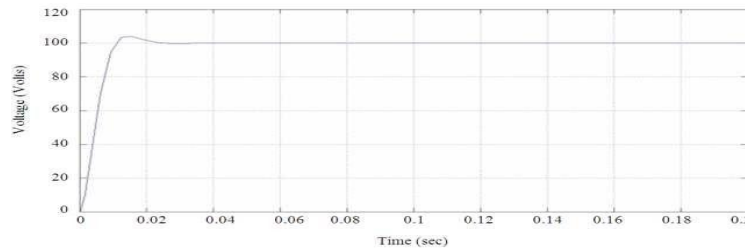


Fig. 15: DC capacitor voltage

DISCUSSION

In this study, a fuzzy logic based current controller strategy is used to regulate the filter current to ensure harmonic free supply current. The simulation is carried out in the MATLAB/SIMULINK environment and the performance was analyzed in a sample power system with a source and a diode rectifier with a R load as a non-linear one. Fuzzy Logic Controller (FLC) Model provides comparatively better harmonic reduction than the conventional PI Controllers and the reactive power requirement from the source has been reduced and the input power factor is been improved.

CONCLUSION

A fuzzy logic based current controller strategy is used to regulate the filter current to ensure harmonic free supply current. The active filter was simulated using MATLAB/SIMULINK and the performance was analyzed in a sample power system with a source and a non-linear load. For power quality control, a Fuzzy Logic Controller (FLC) Model provides comparatively better harmonic reduction than the conventional PI Controllers. The FLC based controller has quick response and more robust than other conventional nonlinear controllers. The simulation results show that for the given system the proposed controller reduces total harmonic distortion below the value recommended by IEEE 519 standard.

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