

A New Approach for Three Phase Grid Connected System with Distributed Generation Systems

P V Samrat & G.Isaac

M.E., College of Engineering,Osmania University M.Tech(Power Electronics and Industrial Drives), JNTU College Of Engg, Hyd

Currently **ABSTRACT:** distributed technology systems are extensively inhabiting there vicinity within the strength generation.Gridcodes from the transmission machine operatorspronounce the behaviour of the strength supply, regulating voltage limits and reactive powerinjection to stay linked and supports the gridunder fault. Happening the basis that in contrast to sorts of voltage sags require *different voltage supportstrategies, a flexible manage* scheme for three phasegrid-related inverter is proposed here. For thethree segment balanced voltage sags, the invertershould inject reactive electricity on the way to increase thevoltage in all levels. In one-phase or -phasefaults, the main situation of the DG inverter is toequalize voltages by means of reducing the negative symmetric collection and clean the phase leap. Owingto system obstacles, a stability among those two extreme regulations is obligatory. Thus, over voltageand under voltage may be averted, and the proposed control scheme prevents disconnection whileachieving the desired voltage support service. Thechief contribution of this paintings is the introduction of a control algorithm for reference currentgeneration that provides bendy voltage supportunder grid faults.

KEYWORDS-Distributed Generation Inverters Reactive power manage, voltage sag, voltage support

I. INTRODUCTION

Renergy sources are being broadly used now adays Three for strength generation. segment inverterimplemented inside the unified manage strategy is powerful and gives the higher inductor modern [1]. Distributed era(DG) is rising as a possible alternative whilst renewable ornonconventional energy sources are available, which includes windturbines, photovoltaic arrays, gas cells, micro turbines [2], [4].Most of those assets are

related to the application throughpower electronic interfacing converters, i.E., three-phaseinverter. Moreover, DG is a suitable form to offer high reliableelectrical energy deliver, as it can perform both in thegrid-tied mode or inside the islanded mode [3]. In the grid-tiedoperation, DG deliveries power to the application and the localcritical load. Upon the incidence of application outage, theislanding is fashioned. Under this circumstance, the DG must betripped and end to energize the part of software as quickly aspossible according to IEEE Standard 929-2000 [5]. However, as a way to improve the power reliability of a few neighborhood criticalload, the DG need to disconnect to the software and retain tofeed the neighborhood criticalload [6]. The load voltage is fundamental difficulty of those two operationmodes, because it's far fixed by using the application within the grid-tiedoperation, and formed by using the DG inside the islanded mode, respectively. Therefore, upon the going on of lonely i.E., islanding, DG must take over the load voltage as soon aspossible, in order to reduce the transient inside the load voltage.And this difficulty brings a venture for the operation of DG.Droop-based manipulate is used extensively for the energy sharing of parallel inverters [12], [13], that is known as as voltage modecontrol on this paper, and it is able to also be applied to DG torealize the electricity sharing between DG and utility in the gridtied mode [14]. In this situation, the inverter is alwaysregulated as a voltage supply by way of the voltage loop, and thequality of the load voltage can be guaranteed throughout thetransition of operation modes. However, the limitation of thisapproach is that the dynamic overall performance is terrible, due to the fact thebandwidth of the outside energy loop, figuring out hunch manage, is a lot lower than the voltage loop. Moreover, the gridcurrent isn't always managed directly, and the difficulty of the inrushgrid current all through the transition from the islanded



mode tothe grid-tied mode usually exists, despite the fact that phase lockedloop (PLL) and the virtual inductance are adopted. In thehybrid voltage and contemporary mode manage, there's a need toswitch the controller when the operation mode of DG ischanged. During the c language from the incidence of utilityoutage and switching the controller to voltage mode, the loadvoltage is neither fixed by means of the software, nor regulated through the DG,and the period of the time c program languageperiod is decided by using theislanding detection method. Therefore, the main problem in thisapproach is that it makes the great of the load voltageheavily reliant on the speed and accuracy of the islandingdetection approach [7]-[11].

This paper proposes a unified control method that avoids he aforementioned shortcomings. First, the traditionalinductor modern-day loop is employed to manipulate the Neutral pointclamped (NPC) inverter with a greenback converter which gives neutral factor within the dc voltage in DG to behave as a contemporary sourcewith a given reference in the synchronous reference frame(SRF). Second, a unique voltage controller is presented to supply reference for the inner inductor modern loop, wherein aproportional-plus-quintessential (PI) compensator and a proportional(P) compensator are employed in D-axis and Q-axis, respectively. In the grid-tied operation, the weight voltage isdominated by way of the application, and the voltage compensator in Daxis is saturated, whilst the output of the voltage compensatorin Q-axis is forced to be 0 by way of the PLL. Therefore, thereference of the internal modernday loop cannot regulated through thevoltage loop, and the DG is controlled as a cutting-edge supply justby the internal current loop. Upon the occurrence of the gridoutage, the burden voltage is no greater decided with the aid of the utility and the voltage controller is routinely activated toregulate the burden voltage. These take place obviously, and, thusthe proposed control method does now not want a compelled switchingbetween two awesome sets of controllers. Further, there may be noneed to stumble on the islanding speedy and correctly, and theislanding detection method is no extra vital in thisapproach.

In Fig.1, a block diagram of the controllerfor DG inverters underneath grid fault is shown. The inputsof the controller are the measured phase voltages v atthe PCC, the currents i flowing thru Li inductor, and the dc-link voltage Vdc. Voltage v and modern I am transformed into SRF values. Voltages v α and V β are then decomposed into symmetric additives usinga collection extractor.

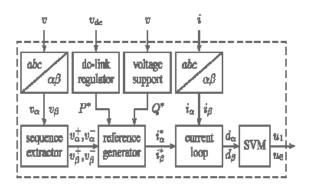


Fig 1. Control diagram of three-phase DG inverterunder grid fault

II. PROPOSED STRATEGY

Under grid connected operation DG should beshould be synchronized with the grid. In this modeeach DG inverter works for the system by themeasured voltage and desired power levels. For unitypower factor operation, it is essential that the gridcurrent reference signal is in phases with the gridvoltage. Current controller design using FlexibleVoltage Support Controller is shown in fig.2

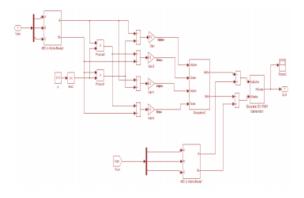


Fig 2 Controller Design

2. Point of Common Coupling



e-ISSN: 2348-6848 p-ISSN: 2348-795X Volume 04 Issue 10 September 2017

The PCC is a factor in the electrical systemwhere multiple clients or multiple electrical loadsmay be linked. In step with IEEE-519, this shouldbe a factor which is accessible to both the software and thecustomer for direct size. Even though in manycases the percent is considered at the metering point, carrier front or facility transformer, IEEE-519states that "inside an commercial plant, the % is thepoint between the non-linear load and different loads."% at service front, metering factor or facilitytransformer it'll normally be less difficult to meetharmonic distortion limits when the % is considered at the metering factor, facility transformer or serviceentrance.

In maximum cases, the present day flowing at thispoint represents a mixture of natural fundamentalcurrent flowing to linear hundreds and each fundamentaland distorted modern flowing to non-linear loads. The distortion current will regularly be a smaller percent of the overall (mixed) essential modern at this point.p.c inside the plant and between the non-linear and linear loads thinking about the % on the gadget will often meet the IEEE-limits each at this factor and also a percent near the provider entrance. The IEEE-519 limitat this factor, which is basically on the enter to the non-linear masses, is regularly 12%, 15% or maybe 20% THD-I.

The ratio of quick circuit present day to loadcurrent is usually plenty large at this %, whichtypically has much less total load, than on the metering factor,where the complete plant load is attached. Usually, if thethd restrict is met at every non-linear load inside theplant, the TDD limits at the carrier entrance can even

Be met. Even though the THD limits are typicallylower for the p.c considered near the software meteringpoint, the overall THD at this p.c can also beconsiderably lower if there are additional linear loads n the plant that percentage the energy supply.

Filter out: The rectifier circuitry takes the initial ac sinewave from the transformer or different source and converts it to pulsating dc. A complete-wave

rectifier willproduce the waveform shown to the proper, while a halfwave rectifier will pass only each different half-cycle toits output. This will be appropriate sufficient for a basic batterycharger, even though some styles of rechargeable batteriesstill may not love it. In any case, it's far nowhere close to goodenough for maximum digital circuitry.We need a manner to easy out the pulsationsand provide a far "cleaner" dc strength supply for theload circuit. To accomplish this, we need to use acircuit called a clear out. In wellknown terms, a filter is anycircuit on the way to dispose of a few components of a signal or powersource, at the same time as permitting other parts to keep onwithout full-size problem. In a power supply, the filter ought to remove or considerably lessen the acvariations while nonetheless making the desired dc available tothe load circuitry.

Filter out circuits are not normally verv complex, however there are several versions. Any given filter mayinvolve capacitors, inductors, and/or resistors in somecombination. Every such mixture has bothadvantages and downsides, and its personal variety of practical utility. If we vicinity a capacitor at theoutput of the overall-wave rectifier as proven to the left, the capacitor will charge to the peak voltage every halfcycle, after which will discharge greater slowly via theload whilst the rectified voltage drops back to zerobefore beginning the following 1/2cycle.hence, the capacitor enables to fill within the gapsbetween the peaks, as shown in pink in the first determine tothe right. Even though we've used directly strains forsimplicity, the decay is surely the everyday exponentialdecay of any capacitor discharging thru a loadresistor. The volume to which the capacitor voltagedrops relies upon at the capacitance of the capacitor and the amount of current drawn by using the load; those twofactors efficaciously shape the RC time consistent forvoltage decay. As a result, the actual voltage output from this mixture never drops to zero, but rathertakes the shape shown inside the 2d discern to the right. The blue part of the waveform corresponds to theportion of the enter cycle where the rectifier providescurrent to the load, whilst the red portion shows when he capacitor gives contemporary to the burden.



III. SIMULATION RESULTS

1. Over All Simulation Diagram with Symmetrical Fault

The modelling of the system with flexiblevoltage support control is designed in simulink. Thegain parameters of flexible voltage support controllerobtained by proper tuning.

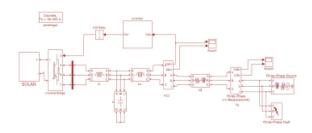


Fig.3 Simulation Diagram with SymmetricalFault Flexible voltage supportcontrol works as a regulator of the voltage and currentduring transition from grid connected to SymmetricalFault. α and β for flexible voltage support control ischosen proper tuning. The Overall Simulation Diagramwith Flexible Voltage Support controller Fig 3.

2. Over all Simulation Diagram withUnsymmetrical Fault

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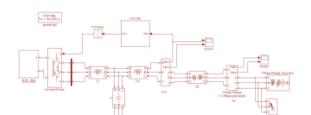


Fig.4 Simulation Diagram withUnsymmetrical Fault

3. Grid Voltage and current for symmetrical fault

The grid voltage and current waveforms without fault is shown Fig.6. The grid voltage is 565 Vand current value is 25 A.

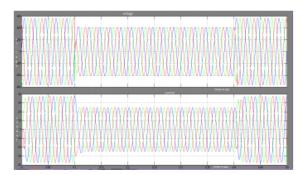


Fig.5 Grid Voltage and Current forsymmetrical Fault

The Fig.5 shows the voltage and current valueof grid and interconnection of solar power plant andthree phase conventional source. In the Fig.5normal condition the voltage and current values arecalculated by using voltage current measurement. Innormal condition with any disturbances grid voltagevalue 400V and current value is 38A in grid.

4. Grid Voltage and current forUnsymmetrical fault

The grid voltage and current waveforms without fault is shown Fig. 6. The grid voltage is 560V and current value is 40A. The Fig. 6 shows the voltage and current value of grid and interconnection of solar power plant and three phase conventional source.



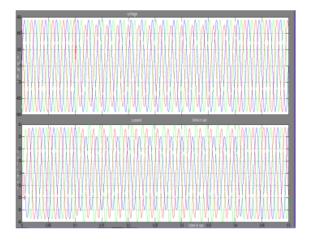


Fig.6 Grid Voltage and Current forsymmetrical Fault

In the Fig 6, Unsymmetrical condition the voltage and current values are calculated by using voltage current measurement. Here R&Y phases are fault condition. The grid voltage value in RY&B phases -565V perphase and grid current value in B phase 40A in R&Y phases 38A. So reduces the fault current values with inlimit using reactive power injection in normal condition.

IV. CONCLUSION

The voltage supportstrategy can be changed by a controlparameter in line with the kind of voltage sag. In threephase balanced sags, the best answer appears to be toraise the voltage in all stages. In one or two-phasefaults, voltage equalization is a desired choicebecause conventional strategies can cause overvoltageand motive disconnection. When the sag is less deep, abalance among those intense guidelines need to beimplemented.

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e-ISSN: 2348-6848 p-ISSN: 2348-795X Volume 04 Issue 10 September 2017

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Authors Details:



P V Samrat completed M.E. from College of Engineering,Osmania University in the year 2013. My areas of Interests are Power Electronics,Power Quality,Grids.



G.Isaac Having 9+ Years Of Exp As Asst Professor In The Dept Of Electrical And Electronics Engg, Presently Working As Asst Professor In Global Institute Of Engg And Technology, Jntu, Hyderabad. I Did B.Tech From Royal College Of Engg (Presently Hyderabad Inst Of Engg And Technology And Management In The Year 2005 And M.Tech (Power Electronics And Industrial Drives) From Jntu College Of Engg Hyd In Year 2010.