

# Improvement In Active Filter Capabilities Of Doubly Fed Induction Generator Using Fuzzy Logic Controller

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**Abstract** -This paper deals with improvement in Doubly Fed Induction Generator (DFIG) by using FLC based on control of Grid-Side Converter (GSC).GSC does mainly two things which are very useful to the system to maintain stability: One is Slip power transfer and the other is supply of harmonics which is useful to mitigate the harmonics produced due to nonlinear loads at PCC. The Rotor-Side Converter (RSC) mainly does the power extraction which is called MPPT (Maximum Power Point Tracking) and also for supplying sufficient reactive power to DFIG. In this paper, FLC is used instead of using other controllers because it is best acceptable for the animal controlling mechanism, accouterment the operation of making decisions with experts. This Wind Energy Conversion Arrangement (WECS) acts as a STATCOM for giving harmonics, even though wind turbine not able to operate/shutdown condition. GSC and RSC control algorithms are explained in brief. The DFIG which is based on WECS is explained using the MATLAB/Simulink. By application of FLC for a nonlinear arrangement allows reducing the uncertain effects developed at nonlinear loads also improves the efficiency. The control action for DFIG based WECS is analyzed by simulation results.

**Key Terms** - Doubly Fed Induction Generator, Integrated Active Filter, Fuzzy Logic Controller, Nonlinear Load, Power Quality, Wind Energy Conversion System.

## I.INTRODUCTION

With raise in population and industrialization, the power demand consumes been increased considerably. Though, the renewable sources of energy like oil, coal and gas are limited in nature. At the moment conventional sources are very important [1]. These are mainly used since it is apt for nature and it will not harm any environment. [2]. since the technical enhancements, the price of wind energy generated is analogous to renewable sources. Nowadays, several load area units are powered by conventional sources and controlling action is doubly using the Fuzzy Logic Controller.

With the advanced power electronic devices, machine can run at adaptable speeds. DFIG is chosen due to its low price compared to all other wind turbines operated at different speeds. One other advantage of Double Fed Induction machine is the maximum energy output, minimum convertor rating, and better utilization of generators.

The better damping performance at weak grid is also provided by DFIG. The reactive power and active power is received separately with the decoupled vector control

algorithm the vector control algorithm of system is commonly apprehended through synchronously revolving reference frame concerned with voltage axis or with flux axis. Rotor-Side Converter (RSC) controlling action is applied by voltage-oriented reference scheme. The requirements for Grid side connections and action of wind sources are discussed.

DFIG response is dependent of Wind Energy Conversion System (WECS) with respect to grid disorder. Since wind diffusion in the grid becomes significant, the usage of different speed WECS for supplementary jobs like power smoothening and harmonic alleviation are compulsory added to its power extraction. It is achieved by summing of super magnetic energy storage systems which are discussed. The other supplementary services like transient stability boundary and reactive power condition are obtained by using static compensator (STATCOM).

The fly-wheel energy storage system along with DSTATCOM (Distribution STATCOM) together at the wind energy source is used to reduce harmonics and to reduce disturbance in frequency. For better power quality and reliability, the DC link with super capacitor energy storage device established. For the methods which are discussed above, for reactive power control and for reducing harmonics GSC and RSC are used. maximum power extraction and the reactive power compensation can be achieved with the help RSC. Therefore, the rotor part receives harmonics from RSC which makes noise and disturbances in the system, the motorized disturb may also be created due to harmonics injection in rotor windings. Due to this reason the RSC rating is increased significantly. SC is used for controlling the reactive power of DFIG and PWM generator generates the pulses without any disturbance by exploitation the fuzzy controller.

Harmonic compensation is done by GSC, so that the harmonics do not enter to the machine windings which in turn keep the equipment safe. An Indirect current control algorithm which is a new control algorithm have been used for reducing harmonics obtained through nonlinear loads at Grid Side Converter

The most and interesting factor of DFIG is it supplies energy even turbine is in not operate able position /shutdown

condition and after that it reimburses harmonics and load reactive power at turbine stopping case. DFIG is explained at different wind speed conditions and at unbalanced nonlinear loads at Point of Common Coupling (PCC).

## II. PRINCIPLE OF DFIG

In this stator part is directly linked to grid, and the rotor part is also connected to grid via through dc-link and the RSC & GSC converters, due to this reason it is called as DOUBLY FED INDUCTION MACHINE as shown below in figure 1.

Figure shows the WECS along with combined active filter capabilities with two end-to-end connected Voltage Source Converters (VSCs) i.e., RSC and GSC are placed between grid and rotor, nonlinear loads are placed at PCC. The generalized DFIG functions like active filter along with supply of active power generation as of normal DFIG.

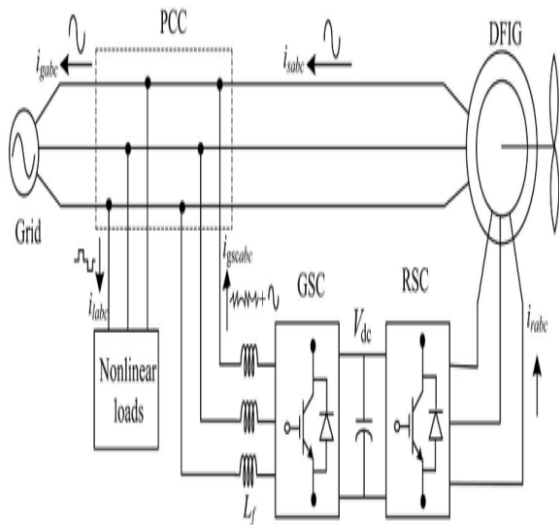


Fig. 1. General diagram of DFIG

Harmonics which are generated through nonlinear loads are interlinked at the PCC distort at the PCC voltage. GSC control can be reduced by these type of nonlinear load harmonic currents, by this we can eliminate the stator coil and grid currents, and also make them harmonic-free. To achieve Maximum Power Point Tracking (MPPT) we need to control RSC and by creating this we can achieve unity power factor at the stator side by using referenced voltage-oriented frame.

## III. BASED ON WECS THE STRATEGY OF DFIG

Selection of dc-link voltage and VSCs ratings is an vital role for the good functioning of WECS. Dc-link voltage selection depends on rotor voltage and on PCC voltage, when we consider DC-Link voltage selection by rotor side, then the voltage of rotor is slip times than voltage of stator. The DFIG which is based on WECS selection implemented in model has ratio =2:1. i.e., stator to rotor turns=2:1. Hence forth estimated dc-link voltage given as

$$V_{dc} \geq \frac{2\sqrt{2}}{\sqrt{3+m}} V_{ab} \quad (1)$$

Here V<sub>ab</sub>=PCC line voltage

Maximum Modulation Index(MMI)can be chosen 1 for the linear range. Then dc-link voltage (V<sub>dc</sub>) is estimated as 375 V.

Selecting VSC Rating and the lagging volt-ampere reactive (VAR) can be drawn with DFIG for the excitation, and rated air gap voltage is built across the system. By using this, we can calculate V<sub>ab</sub> by machine parameter but we need lagging VAR about 2 KVAR to run it as motor.

Therefore, we can find VSC rating which is used on RSC S<sub>rated</sub>as shown in below equation.

$$S_{rated} = \sqrt{P_r^2 + Q_r^2} \quad (2)$$

Hence, kVA rating of RSC S<sub>rated</sub> is estimated to value 1.615 kVA.

Design pattern of the Interfacing Inductor, and design of the interfacing inductors is given in amidof PCC and GSC which depends on maximum limit of GSC current which is also called (i<sub>gscpp</sub>), voltage of dc-link selection, and also switching frequency component of GSC. Max amount of line current is depending on mostly max power and line voltage in GSC. Possibility of extent power in GSC is slip power.

In this case we consider the, the slip power considered as 1.5 kW,Line voltage (VL) at the GSC is 230 V (Which means machine is in delta mode). The value of an inductor is given as

$$L_i = \frac{3 \text{ mV}_{dc}}{12 a f_m \Delta i_{gsc}} = \frac{3 \times 10000 \times 0.25 \times 3.76 \times 1 \times 375}{12 \times 1.5 \times 3.76} = 3.8 \text{ mH.} \quad (3)$$

$$L_i = \frac{\sqrt{3} \text{ mV}_{dc}}{12 a f_m \Delta i_{gsc}}$$

$$= \frac{\sqrt{3} \times 1 \times 375}{12 \times 1.5 \times 10000 \times 0.25 \times 3.76} = 3.8 \text{ mH.} \quad (3)$$

Finally, the interfacing inductor (L<sub>i</sub>)in-between GSC and PCC iscalculated as 4 MH.

## IV. FUZZY LOGIC CONTROLLER

In FLC set linguistic rules are taken for determining basic control action. These rules are determined by using of system Because in this type the mathematical variables are converted to linguistic variables to make it understand by FLC system, the main benefit of this system is mathematical modeling is not required in FLC. The FLC mainly consist of 3 parts: interference engine, fuzzification and defuzzification. FC is mainly categorized as below

i. Fuzzificationby means of continuous universe of discourse.

ii.Defuzzification using the height method.

iii.Seven fuzzy sets for each input and output.

iv.. It includes the simple Triangular membership rules.

v. Implication using Mamdani's, 'min' operator.

**TABLE II**Fuzzy Rules

| Change in error | Error |    |    |    |    |    |    |
|-----------------|-------|----|----|----|----|----|----|
|                 | NB    | NM | NS | Z  | PS | PM | PB |
| NB              | PB    | PB | PB | PM | PM | PS | Z  |
| NM              | PB    | PB | PM | PM | PS | Z  | Z  |
| NS              | PB    | PM | PS | PS | Z  | NM | NB |
| Z               | PB    | PM | PS | Z  | NS | NM | NB |
| PS              | PM    | PS | Z  | NS | NM | NB | NB |
| PM              | PS    | Z  | NS | NM | NM | NB | NB |
| PB              | Z     | NS | NM | NM | NB | NB | NB |

**Fuzzification:**

The linguistic variables are assigned to the values of Membership function by using seven fuzzy subsets: Negative Big, Negative Medium, Negative Small, Zero, Positive Small, Positive Medium and Positive Big. Division of fuzzy are part of the shape of membership CE(k) E(k) function and they adjust to the form up to appropriate system. scaling factor plays a vital role in worth of input fault and alter in error caused due to input error are minimized by an input .

In input scaling factor has been designed in a form that input values are between the range -1 and +1.

Triangular shape which is as membership function of this collection indicate that there is only one leading fuzzy subsection for particular E(k) input. The input error can be given for FLC as

$$E(k) = \frac{P_{ph(k)} - P_{ph(k-1)}}{V_{ph(k)} - V_{ph(k-1)}} \quad (22)$$

$$CE(k) = E(k) - E(k-1) \quad (23)$$

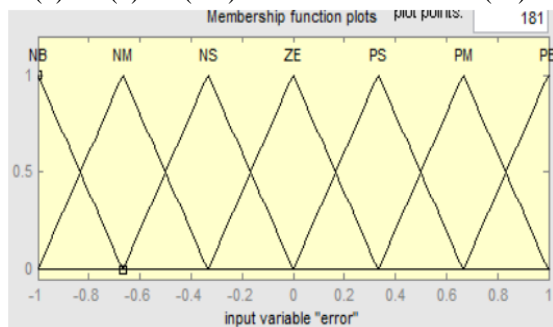


Fig.7.Membership Functions

**Inference Method:**

Different type of mixed methods like Max–Min and Max-Dot is introduced in the text. In this scenario the method used is Min method. Minimum operator and Maximum operator are used as output membership function. Table indicate that the rule base on the FLC.

**Defuzzification:**

A plant mostly needs non-fuzzy standards to have control completely, In Defuzzification phase is must obtain output of Fuzzy Logic Controller(FLC) that is “height” a method function is used to obtain output of FLC which modifies the output control. Thereafter, inverter switch controls FLC output to get the efficient output. In Unified Power Flow Controller(UPFC), terminal voltage, reactive power and

active power, of line and voltage at capacitor must be maintained with proper value. In order to control these bound terminal voltage, reactive power and active power of line and voltage at capacitor (capacitor voltage vc) are detected and associated with their reference values. To obtain this, membership functions in FLC are: input error and differential error i.e., change in error caused due to input error and output. The set of FC rules can be derived from

$$u = -[\alpha E + (1-\alpha)*C] \quad (24)$$

Here  $\alpha$  = self-adjustable factor i.e., It can control the entire process of the system. Where as E=error of the system, u = control variable, C = difference in error. A large number of error E indicates that the given system is not in a balanced state. If the system considered as an unbalanced system, then the controller should increase its control variables and balance the system as must fast as possible to maintain the system in proper condition. On the other side, the small value of error determines that the system very must near to balanced state.

**V. CONTROL STRATEGY**

RSC and GSC they both have CONTROL STRATEGY AND SIMULATION RESULTS Control algorithms are explained in brief. Complete control strategy schematic is shown in Fig. 2. wind turbine features with Type A chopper and DC-machine are been matched by control algorithm which are also shown in below figure.2.

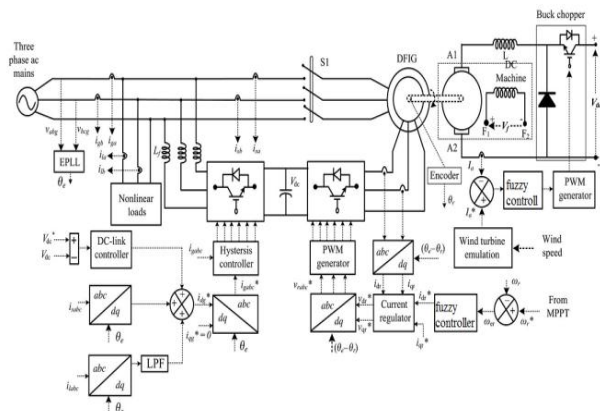


Fig. 2. Control strategy for DFIG based on WECS.

WECS uses the recommended Control algorithm. RSC Direct axis reference rotor current is controlled for obtaining max power for particular wind speed which in turn increases the efficiency and give the maximum output.

**A. RSC Control**

Direct axis reference rotor current is used so that maximum power is extracted for a particular wind speed. The maximum power is obtained by operating DFIG at rotor speed used for a particular wind speed. So, here outer loop is chosen as a speed controller for

$$i_{dr}^*(k) = i_{dr}^*(k-1) + k_{pd}\{\omega_{er}(k) - \omega_{er}(k-1)\} + k_{id}\omega_{er}(k) \quad (4)$$

where the speed error ( $\omega_{er}$ ) is achieved by subtracting sensed speed ( $\omega_r$ ) from the reference speed ( $\omega_r^*$ ).  $k_{id}$  and  $k_{pd}$  are the integral and proportional constants of the PI-speed controller.  $\omega_{er}(k-1)$  and  $\omega_{er}(k)$  are the speed errors at  $(k-1)$ th and  $k$ th and similarly  $i_{dr}^*(k-1)$  and  $i_{dr}^*(k)$  are the direct axis rotor reference current at  $(k-1)$ th and  $k$ th instants respectively. By the optimal tip speed ratio control for the chosen wind speed the rotor speed is calculated on the reference axis ( $\omega_r^*$ ). Here, the controlling action of RSC is handled by using of voltage-oriented reference frame. By regulating direct and quadrature axis rotor currents ( $i_{dr}$  and  $i_{qr}$ ), the active and reactive powers are controlled respectively. To obtain the direct axis reference rotor current ( $i_{dr}^*$ ) as inner current control loops are in use to control the real direct and quadrature axis rotor currents ( $i_{dr}$  and  $i_{qr}$ ). From the detected rotor currents ( $i_{ra}$ ,  $i_{rb}$ , and  $i_{rc}$ ), rotor currents  $i_{dr}$  and  $i_{qr}$  are obtained

$$i_{dr} = 2/3 [i_{ra} \sin \theta_{slip} + i_{rb} \sin(\theta_{slip} - 2\pi/3) + i_{rc} \sin(\theta_{slip} + 2\pi/3)] \quad (5)$$

$$i_{qr} = 2/3 [i_{ra} \cos \theta_{slip} + i_{rb} \cos(\theta_{slip} - 2\pi/3) + i_{rc} \cos(\theta_{slip} + 2\pi/3)] \quad (6)$$

where slip angle ( $\theta_{slip}$ ) is calculated as

$$\theta_{slip} = \theta_e - \theta_r \quad (7)$$

Where  $\theta_e$  is achieved by PLL for aligning rotor currents to voltage axis. The rotor position ( $\theta_r$ ) is obtained with an encoder.

Through Direct and quadrature axis rotor current errors ( $i_{der}$  and  $i_{qer}$ ) the Direct and quadrature axis rotor voltages ( $v_{dr}$  and  $v_{qr}$ ) are obtained

$$v_{dr}'(k) = v_{dr}'(k-1) + k_{pdv}\{i_{der}(k) - i_{der}(k-1)\} + k_{idv}i_{der}(k) \quad (8)$$

$$v_{qr}'(k) = v_{qr}'(k-1) + k_{pdv}\{i_{qer}(k) - i_{qer}(k-1)\} + k_{idv}i_{qer}(k) \quad (9)$$

Where

$$i_{der} = i_{dr}^* - i_{dr} \text{ and } i_{qer} = i_{qr}^* - i_{qr} \quad (10)$$

Where the direct axis current controller of the controller gains are  $k_{pdv}$  and  $k_{idv}$  which are the proportional and integral similarly for the quadrature axis current controller  $k_{pdv}$  and  $k_{idv}$  are the proportional and integral gains. Direct and quadrature components are combined by adding some related terms as

$$v_{dr}^* = v_{dr}' + (\omega_e - \omega_r)\sigma L_r i_{dr} \quad (11)$$

$$v_{qr}^* = v_{qr}' - (\omega_e - \omega_r)(L_m i_{dr} + \sigma L_r i_{dr}) \quad (12)$$

The three phase reference rotor voltages ( $v_{ra}^*$ ,  $v_{rb}^*$ ,  $v_{rc}^*$ ) are obtained by converting these reference direct and quadrature voltages ( $v_{dr}^*$ ,  $v_{qr}^*$ ) to three phase reference rotor voltages ( $v_{ra}^*$ ,  $v_{rb}^*$ ,  $v_{rc}^*$ )

$$v_{ra}^* = v_{dr}^* \sin \theta_{slip} + v_{qr}^* \cos \theta_{slip} \quad (13)$$

$$v_{rb}^* = v_{dr}^* \sin(\theta_{slip} - 2\pi/3) + v_{qr}^* \cos(\theta_{slip} - 2\pi/3) \quad (14)$$

$$v_{rc}^* = v_{dr}^* \sin(\theta_{slip} + 2\pi/3) + v_{qr}^* \cos(\theta_{slip} + 2\pi/3) \quad (15)$$

To obtain pulse-width modulation (PWM) signals to RSC, a comparison is done between three phase rotor reference voltages ( $v_{ra}^*$ ,  $v_{rb}^*$ ,  $v_{rc}^*$ ) and the triangular carrier wave of fixed switching frequency.

By using Ziegler Nichols method RSC and GSC tuning of fuzzy is achieved. Firstly the  $k_{id}$  value is set to zero and the value of  $k_{pd}$  was increased until the result is oscillating with a period of  $T_i$ . Generally, the stator reactive power (Q s) is done zero since the quadrature axis reference rotor current ( $i_{qr}^*$ ) is selected. For the injection of sufficient reactive power the quadrature axis reference rotor current ( $i_{qr}^*$ ) is selected.

### B. GSC Control

Grid Side Converter is mainly used to reduce the harmonics developed by the non linear loads at the Point of Common Coupling (PCC).

The GSC controlling strategy is shown in below figure/ Fig. 2. For making the grid currents balanced and sinusoidal an indirect current is supplied, these indirect currents are harmonics which are given by the Grid Side Converter (GSC). By operating the the dc-link voltage error ( $v_{dce}$ ) in between reference and calculated dc-link voltage ( $V_{dc}^*$  and  $V_{dc}$ ) through fuzzy controller, active power component of GSC current is obtained. The Grid currents is shown in the below equations

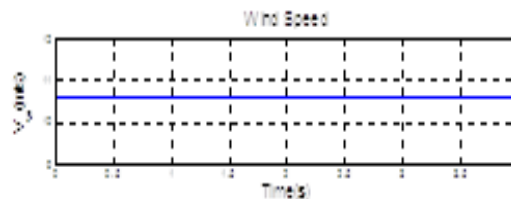
$$i_{gsc}^*(k) = i_{gsc}^*(k-1) + k_{pd}\{v_{dce}(k) - v_{dce}(k-1)\} + k_{id}v_{dce}(k) \quad (16)$$

The  $k_{id}$  and  $k_{pd}$  are integral gains and proportional gains of dc-link voltage controller.  $v_{dce}(k)$  and  $v_{dce}(k-1)$  are dc-link voltage errors at  $k$ th and  $(k-1)$ th instants, Similarly  $i_{gsc}^*(k)$  and  $i_{gsc}^*(k-1)$  are active power component of GSC current at  $k$ th and  $(k-1)$ th instants. By the sensed stator currents ( $i_{sa}$ ,  $i_{sb}$ , and  $i_{sc}$ ) using abc to dq transformation an active component in power of stator current ( $i_{ds}$ ) is obtained.

$$i_{ds} = 2/3 [i_{sa} \sin \theta_e + i_{sb} \sin(\theta_e - 2\pi/3) + i_{sc} \sin(\theta_e + 2\pi/3)] \quad (17)$$

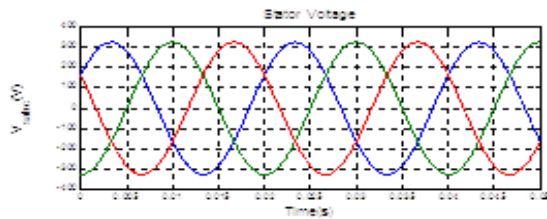
## VI. SIMULATION RESULTS

For various conditions the executed results are as follows

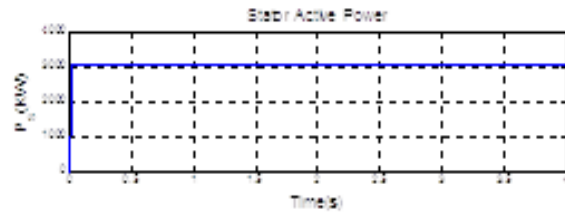


(a)

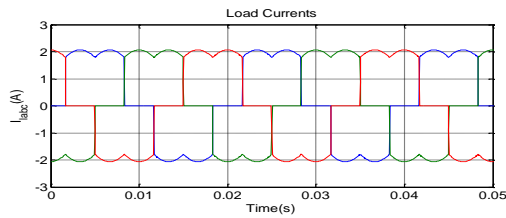




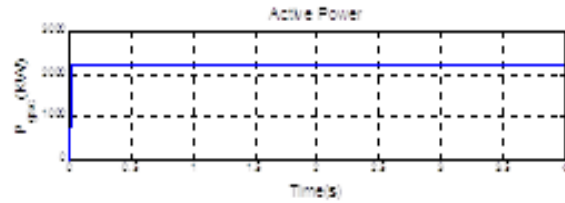
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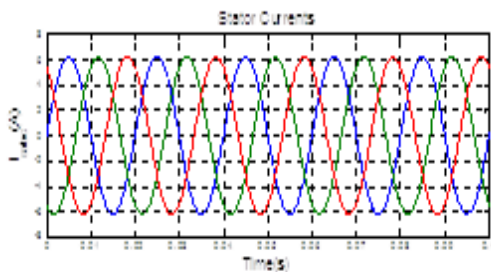
(g)



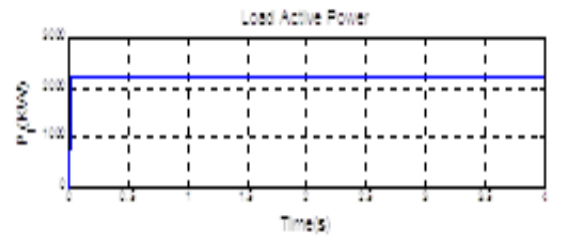
(c)



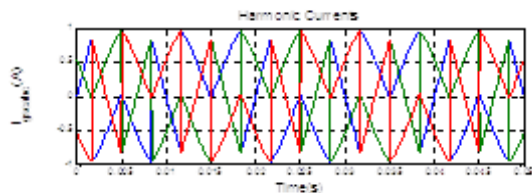
(h)



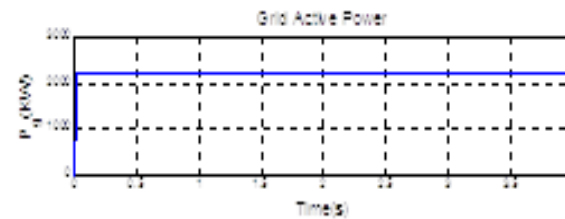
(d)



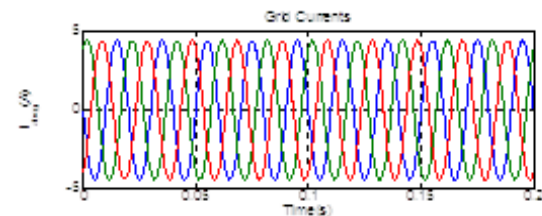
(i)



(e)

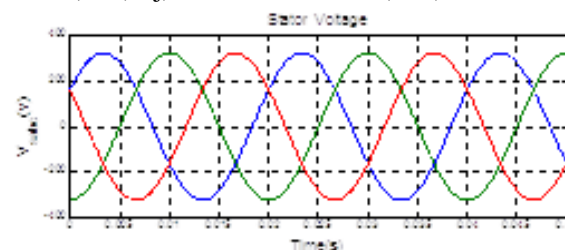


(j)



(f)

Here we can observe that the harmonic currents developed and reduced harmonic waveforms Fig. 3. Simulated results of DFIG-based W ECS at fixed wind speed of 10.6m/s (rotor speed of 1750rpm). (a)-wind Speed(m/s), (b)-Stator Voltage(v), (c)-Load Currents (A), (d)-Stator Currents(A), (e)-harmonic Currents(A), (f)-grid Currents(A), (g)-Stator Currents(A), (h)-Active Power(KW), (i)-Load Active Power(KW), (j)-Grid Active Power(KW)



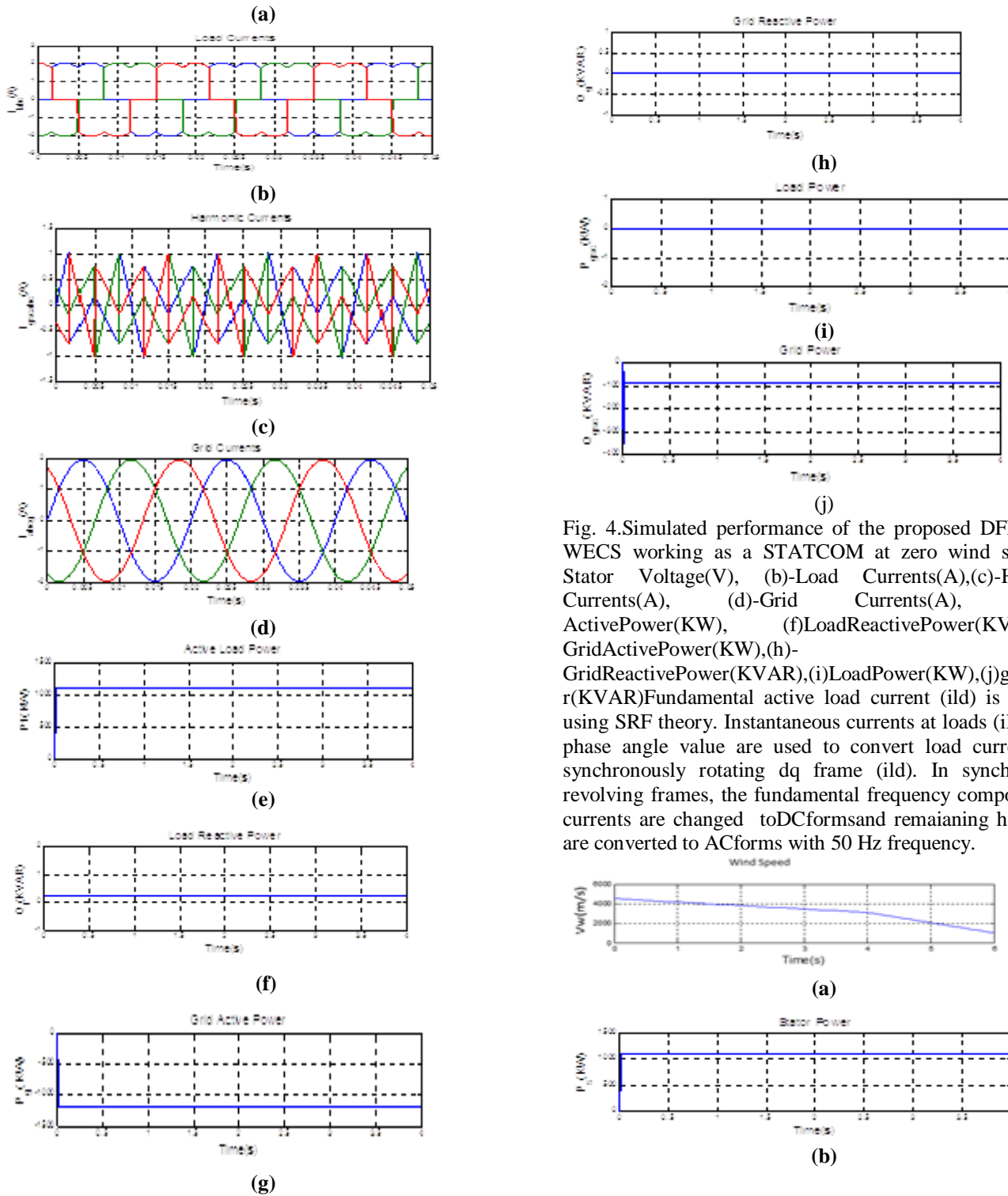
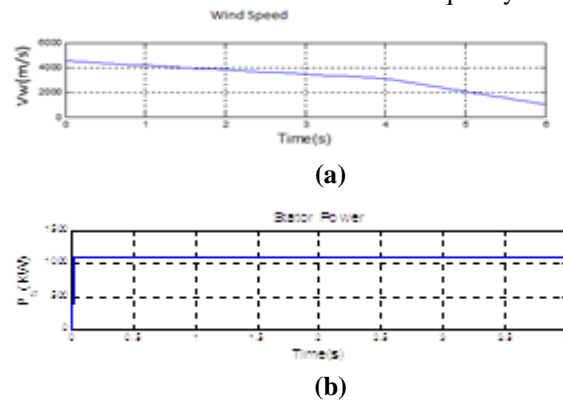


Fig. 4. Simulated performance of the proposed DFIG-based WECS working as a STATCOM at zero wind speed. (a)- Sator Voltage(V), (b)- Load Currents(A), (c)- Harmonic Currents(A), (d)- Grid Currents(A), (e)- Load Active Power(KW), (f)- Load Reactive Power(KVAR), (g)- Grid Active Power(KW), (h)- Grid Reactive Power(KVAR), (i)- Load Power(KW), (j)- grid Power(KVAR). Fundamental active load current ( $i_{ld}$ ) is achieved using SRF theory. Instantaneous currents at loads ( $i_{labc}$ ) and phase angle value are used to convert load currents into synchronously rotating dq frame ( $i_{ld}$ ). In synchronously revolving frames, the fundamental frequency components of currents are changed to DC forms and remaining harmonics are converted to AC forms with 50 Hz frequency.



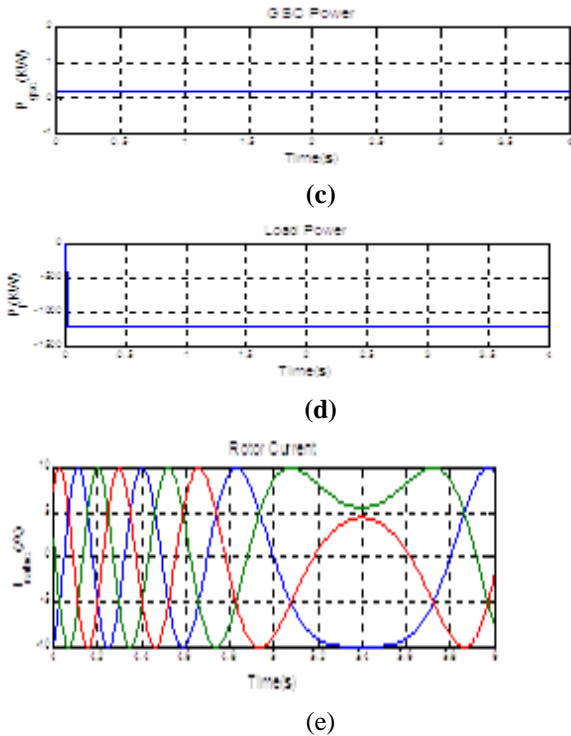


Fig. 5. Waveforms of proposed DFIG for fall in wind speed. (a)-wind Speed(m/s), (b)-Stator Power(KW), (c)-GSC Power(KW), (d)-Load Power(KW), (e)-Rotor Currents(A)

Load current ( $i_{ld}$ ) in the synchronously revolving frame and loss component of current at GSC ( $i_{gsc}$ ) is shown in below equation as

$$i_{ga}^* = i_{gsc}^* + i_{ds} - i_{ld} \quad (18)$$

Load currents of Direct currents values in synchronously revolving dq frame ( $i_{ld}$ ) is pulled by means of low-pass filter (LPF). For generating the switching pulses the hysteresis current controller is used. The feedback controller which controls the current in hysteresis controller senses current meets the reference current in a loop of hysteresis band ( $i_{hb}$ ). At every point of instant, the actual current ( $i_{gabc}$ ) is compared to the reference current ( $i_{gabc}^*$ ) as

$$\Delta i_{gabc} = i_{gabc}^* - i_{gabc} \quad (19)$$

When  $\Delta i_{gabc} > i_{hb}$  lower switch is turned ON (20)

When  $\Delta i_{gabc} < -i_{hb}$ , upper switch is turned ON (21)

Using these equations, gating pulses for three phases of GSC are regenerated.

## VI. RESULTS AND DISCUSSION

The results of both simulated and test are explained herefor validating steady-state and dynamic performances of this proposed DFIG with integrated active filter capabilities. (iv)

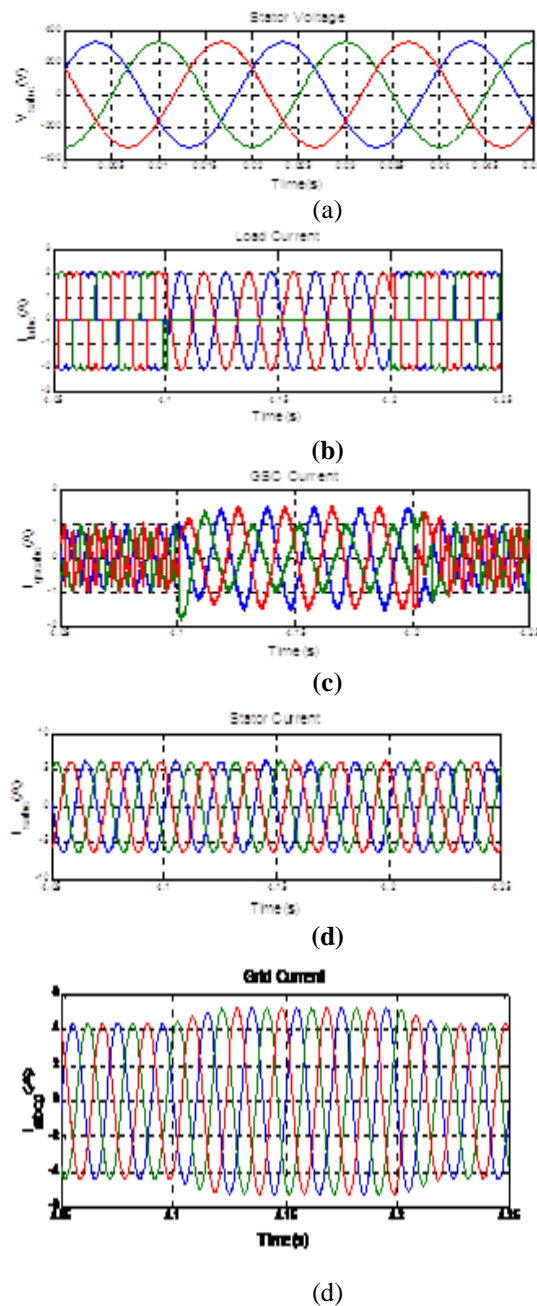


Fig. 8. DFIG-based on WECS when loads are suddenly removed and when used of local loads. (a)-Stator Voltage(V), (b)-Load Currents(A), (c)-GSC Currents, (d)-Stator Currents(A), (e)-grid Currents(A) Here we can observe Stator voltage, Load current, GSC currents, Stator currents, Grid currents waveforms for sudden removal of load.

## VII. CONCLUSION

In recommended DFIG work, the responsive energy of induction machines has provided by means of Rotor Side Converter(RSC) and the load responsive power is

bought by means of Grid Side Converter(GSC). The Grid Side Converter (GSC) algorithm in suggested DFIG has been changed for the contributing reactive power and minimization of harmonics at local loads in proposed DFIG is done by means of Grid Side Converter. Rotor Side Converter(RSC) is mainly helped for the separate control of reactive power and active. The proposed DFIG has been tested at wind turbine stall situation for rewarding harmonics and reactive active power of local loads. This proposed DFIG-based WECS with an combined active filter has been replicated by MATLAB\Simulink environment, and the imitation results are corroborated for different conditions of wind speed and unexpected application of removal of local loads. Steady-state performance and active performance of the DFIG system with the proposed control strategy has been verified for various conditions as mentioned above.

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